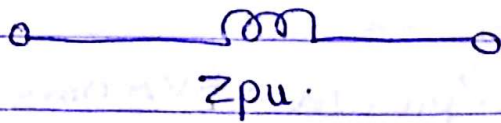


$$Z_{02} \text{ pu} = \frac{Z_{01} (\text{KV}_{B1})}{(\text{KV}_{B1})^2 \times 1000}$$

$$\therefore Z_{01} \text{ pu} = Z_{02} = Z_{\text{pu}}$$



Q Three generators are rated as follows.

Gen 1 : 100 MVA, 33 kV, reactance = 10%

Gen 2 : 150 MVA, 32 kV, reactance = 8%

Gen 3 : 110 MVA, 30 kV, reactance = 12%

Choosing 200 MVA & 35 kV as base quantities, compute p.u reactance of 3 Gen referred to these base quantities, draw reactance diagram & mark p.u reactances. The three generators are connected to common bus-bars.

Gen 1 :

$$\rightarrow X_{\text{pu new}} = X_{\text{pu old}} \times \frac{\text{KVA}_{\text{new}}}{\text{KVA}_{\text{old}}} \times \left(\frac{\text{KV}_{\text{old}}}{\text{KV}_{\text{new}}} \right)^2$$

$$= \frac{10}{100} \times \frac{200 \times 10^3}{1000 \times 10^3} \times \left(\frac{33}{35} \right)^2$$

$$= 0.1777 \text{ pu}$$

Gen 2

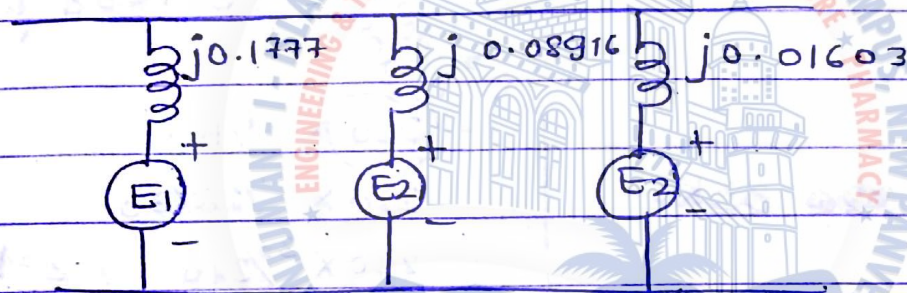
$$\rightarrow X_{pu \text{ new}} = \frac{8}{100} \times \frac{200 \times 10^3}{150 \times 10^3} \times \left(\frac{32}{35}\right)^2$$

$$= 0.08916 \text{ p.u.}$$

Gen 3

$$\rightarrow X_{pu \text{ new}} = \frac{12}{100} \times \frac{200 \times 10^3}{110 \times 10^3} \times \left(\frac{30}{35}\right)^2$$

$$= 0.16029 \text{ p.u.}$$



Q Draw pu impedance diagram for the power system shown. Neglect 'R' & use base of 100 MVA 220 kV in 50 Ω line. The rating of the generator motor, transformer are

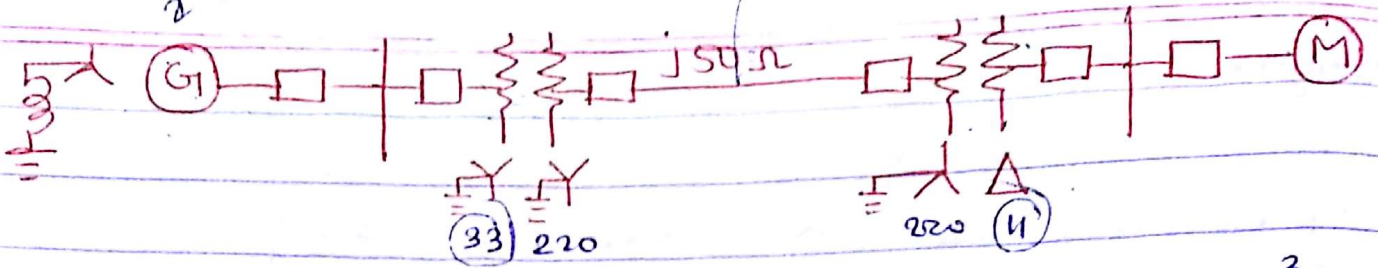
Generator : 40 MVA, 25 kV, $X'' = 20\%$

Motor : 50 MVA, 11 kV, $X'' = 30\%$

Y-Y $X_{mer} = 40 \text{ MVA}, 33\Delta - 220 \text{ Y kV}, X = 15\%$

Y- Δ $X_{mer} = 30 \text{ MVA}, 11\Delta - 220 \text{ Y kV}, X = 15\%$

220/11



→ Base KVA for complete ckt = 100 MVA = 100×10^3 KVA

• Transmission line

→ Base kv = 220 kv.

→ Actual $X = j50 \Omega$

→ X_{pu} of line = $\frac{X_{actual} \times KVA_B}{(KV_B)^2 \times 1000} = \frac{j50 \times 100 \times 10^3}{220^2 \times 1000} = j0.1033 \text{ p.u.}$

• Generator

→ Base kv = ~~220~~ 33 kv.

Base in transmission line = $220 \times 1/kv.$

= $220 \times 1/220/33$

= $220 \times 33/220 = 33 \text{ kv.}$

→ $X_{pu} = \frac{20}{100} \times \frac{100 \times 10^3}{40 \times 10^3} \times \left(\frac{25}{33}\right)^2 = j0.287 \text{ p.u.}$

• Motor

→ Base kv = 11 kv.

= $220 \times k = 220 \times \frac{220}{220} = 11 \text{ kv,}$

= $220 \times 1/220 = 11 \text{ kv}$

→ $X_{pu} = \frac{30}{100} \times \frac{100 \times 10^3}{50 \times 10^3} \times \left(\frac{11}{11}\right)^2 = j0.6 \text{ p.u.}$

Xmer 1 ($\Delta-\Delta$)

220 x 2

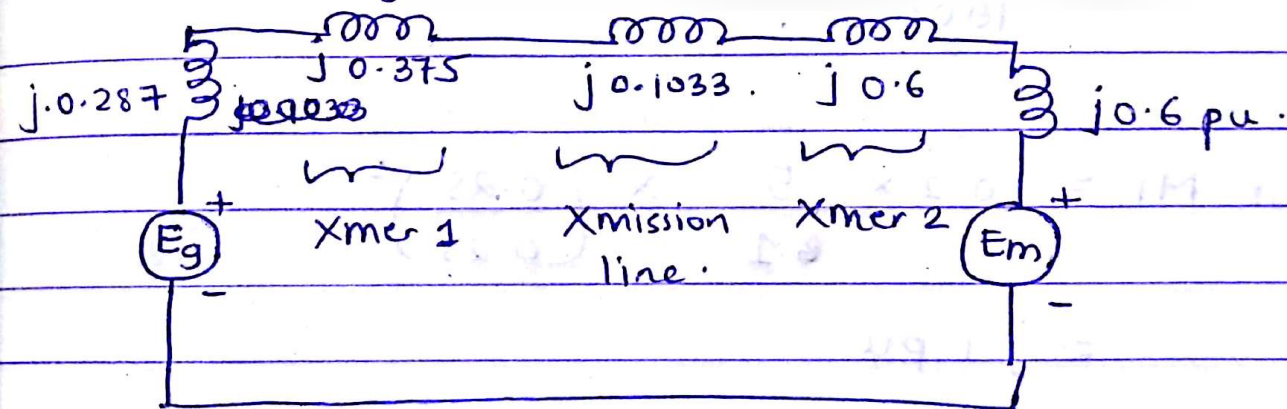
→ Base KV = 33 KV. = ~~220 x 2~~

→ Xpu new = $\frac{15}{100} \times \frac{100 \times 10^3}{40 \times 10^3} \times \left(\frac{33}{33}\right)^2$
 = j0.375 pu

Xmer 2 ($\Delta-\Delta$)

→ Base KV = 11 KV = ~~220 x 2~~

→ Xpu new = $\frac{15}{100} \times \frac{100 \times 10^3}{30 \times 10^3} \times \left(\frac{11}{11}\right)^2$
 = j0.5 pu

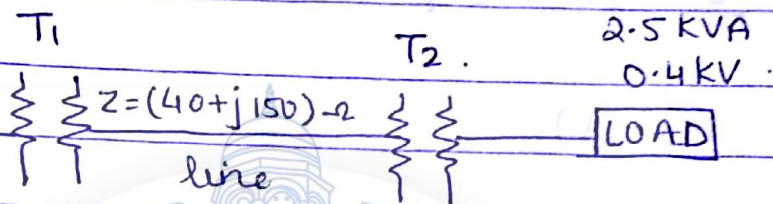


Q A simple power system is shown. Redraw this system where the p.u impedances are represented on a common 5,000 VA base and common system base voltage of 250 V

$$1000 \text{ VA} = 1 \text{ kVA}$$

$$250 \text{ V} = 0.25 \text{ kV}$$

$$\textcircled{1} \quad Z = j0.2 \text{ pu}$$



$$\textcircled{2}$$

$$2000 \text{ VA} = 2 \text{ kVA}$$

$$250 \text{ V} = 0.25 \text{ kV}$$

$$Z = j0.3 \text{ pu}$$

$$\rightarrow \text{Base kVA} = \frac{5000}{1000} = 5 \text{ kVA}$$

$$\rightarrow \text{Base kV} = \frac{250}{1000} = 0.25 \text{ kV}$$

$$\rightarrow X_{pu} \text{ of } M_1 = j0.2 \times \frac{5}{0.1} \times \left(\frac{0.25}{0.25}\right)^2$$

$$= j1 \text{ pu}$$

$$\rightarrow X_{pu} \text{ of } M_2 = j0.3 \times \frac{5}{2} \times \left(\frac{0.25}{0.25}\right)^2$$

$$= j0.75 \text{ pu}$$

$$\rightarrow X_{pu} \text{ of } T_1 = j0.2 \times \frac{5}{4} \times \left(\frac{0.25}{0.25}\right)^2$$

$$= j0.25 \text{ pu}$$

$$\rightarrow X_{pu} \text{ of } T_2 = j0.06 \times \frac{5}{8} \times \left(\frac{0.25}{0.5}\right)^2$$

$$\rightarrow \text{Base voltage in } X_{\text{mission line (TL)}} = \text{Voltage in Gen ckt} \times X_{\text{bormation ratio}}$$

$$= 0.25 \times \left(\frac{0.8}{0.25}\right)$$

$$= 0.8 \text{ kV.}$$

$$\rightarrow X_{pu} \text{ line} = \frac{(40 + j150) \times \text{kVA.B}}{(\text{kV B})^2 \times 1000}$$

$$= \frac{(40 + j150) \times 5}{(0.8)^2 \times 1000}$$

$$= (0.3125 + j1.17) \text{ p.u.}$$

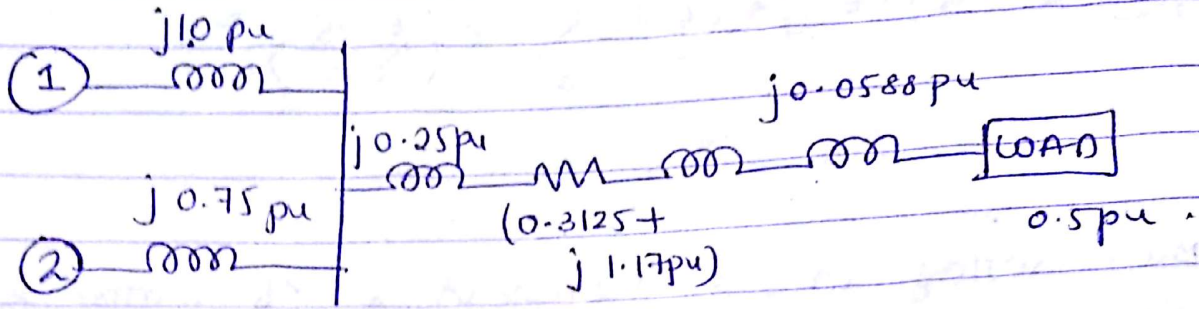
$$\rightarrow X_{pu} \text{ of } T_2 = j0.06 \times \frac{5}{8} \times \left(\frac{1}{0.8}\right)^2$$

$$= 0.0586 \text{ pu.}$$

$$\rightarrow V_B \text{ of TL} = \frac{V_B \text{ of motor ckt}}{K}$$

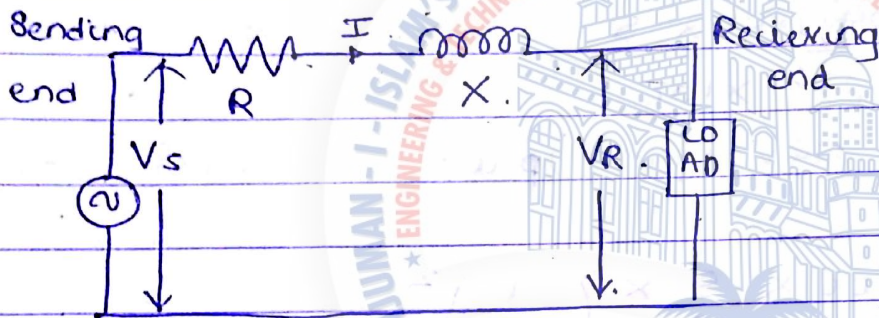
$$= \frac{0.4}{0.5} = \frac{0.4}{0.5} = 0.8$$

$$\rightarrow \text{kVA pu} = \frac{2.5}{5} = 0.5 \text{ pu.}$$



* Short transmission lines :

- Shunt conductance & shunt capacitance is neglected and so only series resistance & inductive reactance is shown.



• From Above;

$$V_R = V_s - I(R + jX)$$

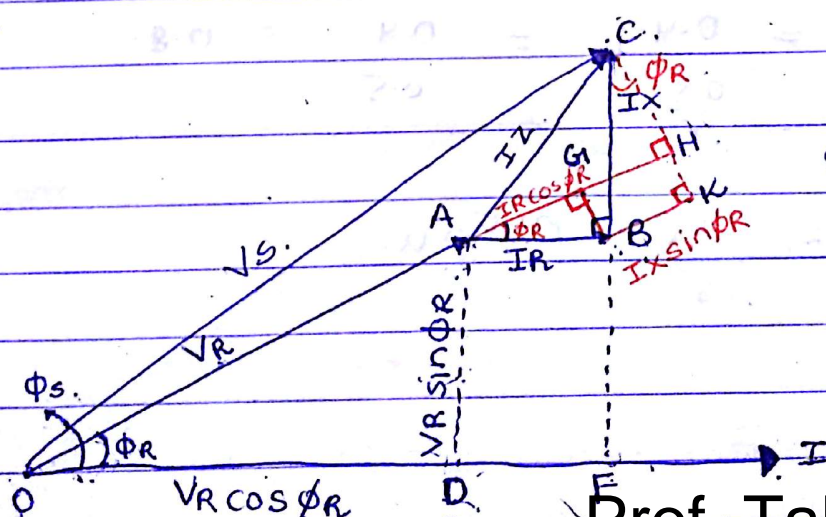
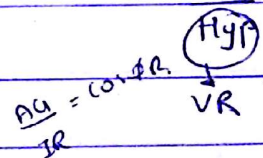
$$= V_s - IZ \rightarrow \text{voltage drop across the line}$$

SHACHOTA

$$\sin \phi_R = \frac{OA}{V_R}$$

$$V_R \sin \phi_R$$

$$\cos \phi_R = \frac{Adj}{Hyp} =$$



(Q) A 200 km long 3 ϕ overhead line has a R of 48.7 Ω /ph, $X_L = 80.20 \Omega$ /ph & $C = 8.42 \text{ nF/km}$. It supplied a load of 13.5 MW at voltage of 88 kV & P.F = 0.9 (lag). Find the $V_S, I_S, V.R, \delta$ (power angle) for (i) Nominal 'T' (ii) Nominal 'TT'

* Nominal 'T' :

$$\rightarrow Z = 48.7 + j 80.20 = 93.8281 \angle 58.732^\circ$$

$$Y = j \omega C l = j 2\pi (50) (8.42 \times 10^{-9}) \times 200 = (5.290 \times 10^{-4}) \angle 90^\circ$$

$$\rightarrow I_{R_{ph}} = \frac{P_R}{\sqrt{3} V_L \cos \phi_R} = \frac{13.5 \times 10^6}{\sqrt{3} \times 88 \times 10^3 \times 0.9} = 98.4119 \text{ A.}$$

$$L = 25.841$$

$$\rightarrow V_R = \frac{V_L}{\sqrt{3}} = 50806.823 \text{ V. } \angle 0^\circ$$

$$\rightarrow V_S = V_R \left(\frac{1 + ZY}{2} \right) + I_R \left(\frac{Z + Z^2 Y}{4} \right)$$

$$= (50806.823 \angle 0^\circ) \left(1 + \frac{(93.8281 \angle 58.732^\circ)(5.290 \times 10^{-4}) \angle 90^\circ}{2} \right)$$

$$+ (98.4119 \angle -25.841^\circ) \left(\frac{93.8281 \angle 58.732^\circ + (93.8281 \angle 58.732^\circ)^2 (5.290 \times 10^{-4}) \angle 90^\circ}{4} \right)$$

$$= 49733.401 \angle 0.7540^\circ + 9136.05 \angle 33.263^\circ$$

$$= 57647.31 \angle 5.6401^\circ$$

phase value
(V_{Sph})

ϕ_1

$$\rightarrow V_S (\text{line}) = \sqrt{3} \times 57647.31 = 99848.07 \text{ V}$$

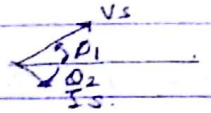
$$\delta (\text{power angle}) = 5.6401$$

$$\rightarrow I_s = V_R (Y) + I_r \left(1 + \frac{ZY}{2} \right)$$

$$= (50806 \cdot 823 \angle 0^\circ) (5.290 \times 10^{-4}) \angle 90^\circ +$$

$$98.4119 \angle -25.841 \left(1 + \frac{(93.828 \angle 58.732)(Y)}{2} \right)$$

$$\therefore 88.3561 \angle (9.095) \rightarrow \phi_{s2}$$



$$\cos(\phi_1 - \phi_2) = \cos(\phi)$$

$$\rightarrow \text{sending end P.F } \cos \phi_s = \cos(5.64 + 9.095) = 0.96711$$

$$\rightarrow V.R = \frac{V_s - V_R}{V_R} \times 100 \%$$

$$= \frac{V_R(\text{no load}) - V_R(\text{full load})}{V_R(\text{full load})} \times 100$$

$$V_R(\text{no load}) = \frac{|V_s|}{\left| 1 + \frac{YZ}{2} \right|} \quad [\because I_r = 0]$$

$$= \frac{|V_{s \text{ phase}}|}{\left| 1 + \frac{YZ}{2} \right|} = \frac{57647.2}{|10.9788 + j0.0127|} = 58890.98 \text{ V}$$

$$V_R(\text{full load}) = 50806.823$$

$$\left(10^{-4} \right) \angle 90^\circ \quad V.R = 0.159 \text{ or } 15.9\%$$

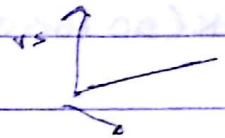
$$\rightarrow \eta = \frac{13.5 \times 10^6}{\sqrt{3} V_{s(\text{line})} I_{s(\text{line})} \cos \phi_s} \times 100$$

$$= \frac{13.5 \times 10^6}{\sqrt{3} (99848.07) (88.3561) \cos(9.095)}$$

$$= \frac{13.5 \times 10^6}{\sqrt{3} (99848.07) (88.3561) (0.96711)}$$

$$= 89\%$$

Deals with phase values.



(* Nominal π)

$$\begin{aligned} \rightarrow V_S &= V_R \left(1 + \frac{ZY}{2} \right) + I_R Z \\ &= 57763 \angle 5.63^\circ \end{aligned}$$

$$\begin{aligned} \rightarrow V_S &= \sqrt{3} \times 57763 = 100 \times 10^3 \text{ V} \\ \delta &= 5.63^\circ \end{aligned}$$

$$\begin{aligned} \rightarrow I_S &= V_R \left(\frac{Y + ZY^2}{4} \right) + I_R \left(\frac{1 + ZY}{2} \right) \\ &= 88.19 \angle -9.29^\circ \end{aligned}$$

$$\begin{aligned} \rightarrow V_R(\text{no load}) &= \frac{|V_S|}{\left| 1 + \frac{ZY}{2} \right|} = \frac{57763}{[0.9788 + j0.0129]} \\ &= 59009.4 \text{ V} \end{aligned}$$

$$\rightarrow V.R = \frac{59009.4 - 50808.3}{50808.3} = 0.16 \text{ or } 16.14\%$$

(Q) A 300km 132kV, 3 ϕ overhead line has a total series impedance of $52 + j200 \Omega/\text{ph}$ & total shunt admittance of $j1.5 \times 10^{-3}$ siemens/ph to neutral. The line is supplying 40 MVA at 0.8 P.F (lag) at 132kV, find V_S , I_S , $\cos \phi_S$, P_S using nominal π circuit.

Q] A 90 MVA, 11 kV, 3 ϕ Generator has $X=25\%$.

$X_{mer T_1}$ is 3 ϕ X_{mer} , 100 MVA, 10/132 kV, $X=6\%$.

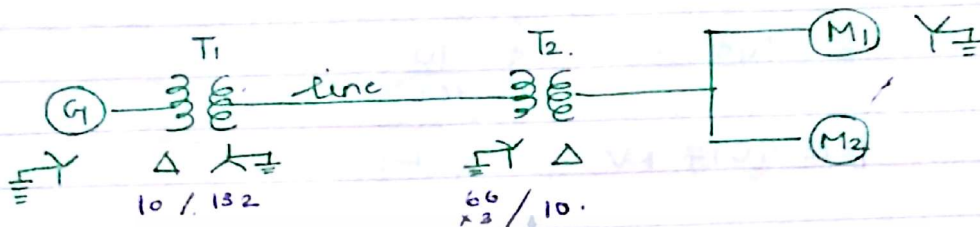
$X_{mer T_2}$ is 1 ϕ -3 X_{mer} , 30 MVA, 66/10 kV, $X=5\%$.

Motor M_1 , 50 MVA, 10 kV, $X=20\%$.

Motor M_2 , 40 MVA, 10 kV, $X=20\%$.

Take Generator rating as Base.

X of line = 100 Ω .



→ Base kVA for complete ckt,
Base kVA = 90×10^3 kVA.

(1) Transmission line:

→ Base kV = 11 kV.

(2) Generator circuit:

Base kVA = 90×10^3 kVA

Base kV = 11 kV.

p.u reactance of Generator = $0.25 \times \frac{90 \times 10^3}{90 \times 10^3} \times \left[\frac{11}{11} \right]^2$
= $j0.25$ or 25%.

(2) Transmission Transformer (T_1):

Base kV = 11 kV = Base kV in generator ckt.

p.u reactance of T_1 = $0.06 \times \frac{90 \times 10^3}{100 \times 10^3} \times \left(\frac{10}{11} \right)^2 = j0.0446$ pu

(3) Transmission line:

Base kV = Base kV (generator) $\times K_{T_1}$

$$= 11 \times \frac{132}{10}$$

$$= 145.2 \text{ kV.}$$

$$I_{line} (\text{Base}) = \frac{\text{kVA base}}{\text{kV Base}} = \frac{90 \times 10^3}{145.2} = 619.834 \text{ A.}$$

$$Z_{line(Base)} = \frac{8V_{base}}{I_{line(Base)}} = \frac{145.2 \times 10^3}{619.234} = j234.256 \Omega$$

p.u 'z' of line = Actual z / Base z = $8100 / 234.256 = j0.427$

(4) Transformer (T2);

$$\text{Base kv (motor ct)} = \text{Base kv (transmission line)} \times k_{T2}$$

$$= 145.2 \times \frac{10}{13766} \rightarrow \text{Note!}$$

$$= 12.7017 \text{ kV}$$

pu reactance of T2 = $0.05 \times \frac{90 \times 10^3}{3230 \times 10^3} \times \left(\frac{12.7017}{12.7017} \right)^2$

$$= j0.0329 \Omega \quad j0.0309 \quad \rightarrow \text{Note!}$$

(5) Motor M1

Base kv in motor ckt = 12.7017 kV.

pu reactance of M1 = $0.2 \times \frac{90 \times 10^3}{50 \times 10^3} \times \left(\frac{10}{12.7017} \right)^2$

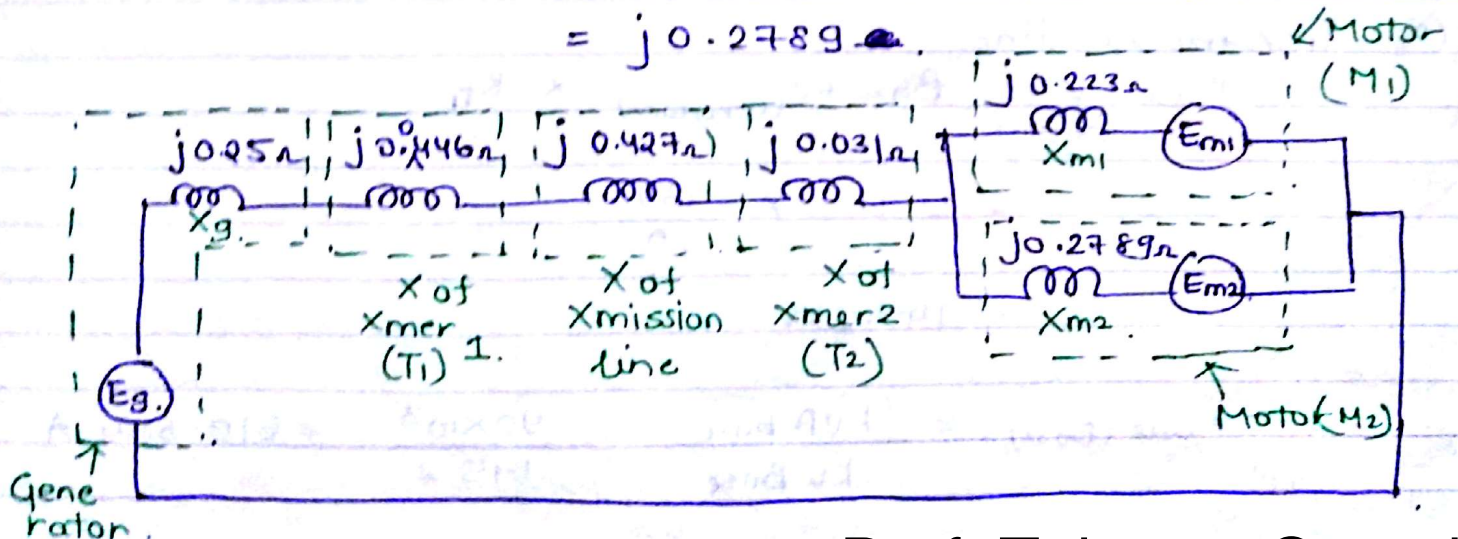
$$= j0.22314 \Omega$$

(6) Motor M2:

Base kv in motor ckt = 12.7017 kV.

pu reactance of M2 = $0.2 \times \frac{90 \times 10^3}{40 \times 10^3} \times \left(\frac{10}{12.7017} \right)^2$

$$= j0.2789 \Omega$$



ratings of generators & transformers are!

G_{11} : 25 MVA, 6.6 kV, $j0.2$ pu.

G_{12} : 15 MVA, 6.6 kV, $j0.15$ pu

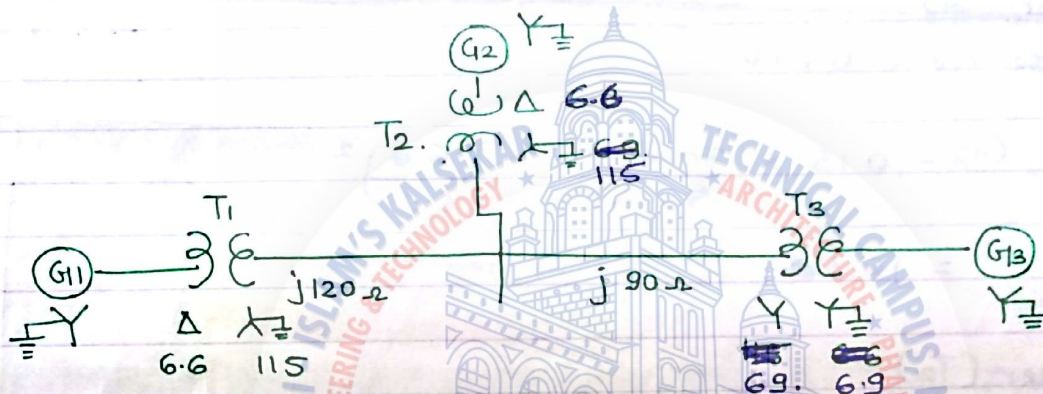
G_{13} : 30 MVA, 13.2 kV, $j0.15$ pu

T_1 : 30 MVA, 6.6 Δ - 115 Y kV, $j0.1$ pu.

T_2 = 15 MVA, 6.6 Δ - 115 Y kV, $j0.1$ pu

T_3 : 1 ϕ - 3 units each rated 10 MVA, 69/6.9 kV, $j0.1$ pu

Base kVA = 30×10^3 } in generator ckt.
Base kv = 6.6



Overall Base kVA = 30 MVA.

(1) Generator G_{11}

Base kVA = 30×10^3 kVA.

Base kv = 6.6 kV

$$\text{p.u. 'x' of } G_{11} = j0.2 \times \frac{30 \times 10^3}{25 \times 10^3} \times \left(\frac{6.6 \times 10^3}{6.6 \times 10^3} \right)^2$$

$$= j0.24$$

(2) Transformer T_1 ;

Base kv = Base kv in generator ckt = 6.6 kV

$$\text{pu 'x' of } T_1 = j0.1 \times \frac{30 \times 10^3}{30 \times 10^3} \times \left(\frac{6.6}{6.6} \right)^2$$

$$= j0.1$$

(3) Xmission line of $j120 \Omega$:

$$\text{Base kv}_{(\text{line})} = \text{Base kv}_{(G_{11})} \times K_{T1}$$

$$= 6.6 \times \frac{115}{6.6} = 115 \text{ kV.}$$

$$I_{\text{line(Base)}} = \frac{\text{KVA (Base)}}{\text{KV base}} = \frac{30 \times 10^3}{115} = 260.869 \text{ A}$$

$$Z_{\text{line(Base)}} = \frac{\text{KV (Base)}}{I_{\text{(Base)}}} = \frac{115 \times 10^3}{260.869} = j440.833 \Omega$$

$$\text{p.u 'Z line' } = \frac{Z_{\text{actual}}}{Z_{\text{Base}}} = \frac{j120}{440.833} = j0.2722$$

(4) Generator G_{12} .

$$\text{Base KV} = 6.6 \text{ KV}$$

$$\text{p.u 'x' of } G_{12} = j0.15 \times \frac{30 \times 10^3}{15 \times 10^3} \times \left(\frac{6.6}{6.6}\right)^2 = j0.3$$

(5) Transformer (T_2)

$$\text{Base KV} = \text{Base KV}_{(G_2)} \times K_{T_2}$$

$$\text{Base KV}_{(T_2)} = \text{Base KV in Generator } (G_{12}) \text{ ckt.} = 6.6 \text{ KV}$$

$$\text{p.u 'x' of } X_{\text{mer}}(T_2) = j0.1 \times \frac{30 \times 10^3}{15 \times 10^3} \times \left(\frac{6.6}{6.6}\right)^2$$

$$= j0.2189 \Omega$$

$$\approx j0.2$$

Use 6.6 KV since Generator is operated at 6.6 KV &

6.9 represents max KV sustained by $X_{\text{mer}}(T_2)$

(6) Generator G_{13} ;

$$\text{Base KV} = 13.2 \text{ KV}$$

$$\text{p.u 'x' of } G_{13} = j0.15 \times \frac{30 \times 10^3}{30 \times 10^3} \times \left(\frac{13.2}{13.2}\right)^2$$

$$= j0.15 \Omega$$

mission line of $j90 \Omega$.

$$\text{Base KV}_{(90\Omega \text{ line})} = \text{Base KV}_{(j100\Omega \text{ line})} = 115 \text{ KV}$$

$$I_{\text{Base}} = \frac{\text{KVA}_{\text{base}}}{\text{KV}_{\text{base}}} = \frac{30 \times 10^3}{115} = 260.8695 \text{ A}$$

$$Z_{\text{Base}} = \frac{V_{\text{base}}}{I_{\text{base}}} = \frac{115 \times 10^3}{260.8695} = j440.8333 \Omega$$

$$\text{p.u. 'Z' of } j90\Omega \text{ line} = \frac{\text{'Z' actual}}{\text{'Z' Base}} = \frac{90}{440.8333} = j0.2041$$

(7) Transformer T_3 ;

$$\text{Base KV}_{(T_3)} = \text{Base KV in } (G_3)$$

$$\text{Base KV}_{(j90\Omega \text{ line})} = \text{Base KV}_{(G_3)} \times K_{T_3}$$

$$115$$

$$= \text{Base KV}_{(G_3)} \times \frac{\sqrt{3} \times 69}{\sqrt{3} \times 6.9}$$

$$\frac{\sqrt{3} \times 6.9}{\sqrt{3} \times 6.9}$$

Note $\times \frac{1}{\sqrt{3}}$

Note $\times \frac{1}{\sqrt{3}}$

$$\therefore \text{Base KV}_{(G_3)} = 11.5 \text{ KV} = \text{Base KV}_{(T_3)}$$

$$\text{p.u. 'x' of } T_3 = j0.1 \times \frac{30 \times 10^3}{3 \times 15 \times 10^3} \times \left(\frac{6.9}{11.5} \right)^2 = j0.072$$

Note!

(8) Generator G_3 ;

$$\text{Base KV}_{(G_3)} = 11.5 \text{ KV}$$

$$\text{p.u. 'x' of } G_3 = j0.15 \times \frac{30 \times 10^3}{30 \times 10^3} \times \left(\frac{13.2}{11.5} \right)^2 = j0.1976$$

