

A PROJECT REPORT
ON
“DESIGN OF VRF SYSTEM”

Submitted by

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In partial fulfillment for the award of the Degree

Of

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UNDER THE GUIDANCE

Of

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ANJUMAN-I-ISLAKALSEKAR TECHNICAL CAMPUS NEW PANVEL,

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A PROJECT
REPORT ON

“DESIGN OF VARIABLE REFRIGERANT FLOW (VRF) SYSTEM”

Submitted to

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In Partial fulfillment of the Requirement for the Award of

Bachelor's degree in Mechanical
Engineering By

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ANJUMAN-I-ISLAM'S KALSEKAR TECHNICAL CAMPUS, NEW PANVEL

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To the Kalsekar Technical Campus, New Panvel is a record of bonafide work carried out by him under our supervision and guidance, for partial fulfillment of the requirements for the award of the Degree of Bachelor of Engineering in Mechanical Engineering as prescribed by **University Of Mumbai**, is approved.

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Project I Approval for Bachelor of Engineering

This Project entitled “*DESIGN OF VRF SYSTEM*” by *Ansari Mohd Uzer, Ansari Mohd Danish, Niwshakar Ayman, Pagarkar Junaid* is approved for the degree of *Bachelor of Engineering in Department of Mechanical Engineering*.

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We declare that this written submission represents our ideas in our own words and where others ideas or words have been included, we have adequately cited and referenced the original sources. We also declare that we have adhered to all principles of academic honesty and integrity and have not misrepresented or fabricated or violation falsified any idea/data/fact/source in my submission. We understand that any violation of the above will be cause for disciplinary action by the Institute and can also evoke penal action from the sources which have thus not been properly cited or from whom proper permission has not been taken when needed.



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ABSTRACT:

Air conditioning demand is rapidly increasing in many parts of the world especially in moderate climate. Air conditioners and refrigerators are the only equipment consumes more electricity say 70 percent house hold articles this result in drastic electricity demands on hot summer days which causes unwanted increase in the use of fossil fuel and nuclear energy which leads to global warming and air pollution. The VRF system uses R410A as refrigerant because it contains only Fluorine hence it has very low global warming potential. VRF systems are enhanced versions of ductless multi-split systems, permitting more indoor units to be connected to each outdoor unit and providing additional features such as simultaneous heating and cooling and heat recovery. VRF technology uses smart integrated controls, variable speed drives, refrigerant piping, and heat recovery to provide products with attributes that include high energy efficiency, flexible operation, ease of installation, low noise, zone control, and comfort using all-electric technology. VRF systems are very popular in Asia.

This thesis presents design of Variable Refrigerant Flow (VRF) system for an office building in Vashi, Navi Mumbai. The VRF system was selected as the space saving was priority of the client. The system is designed using ISHRAE hand book and Toshiba manual. The heat load was calculated considering various factors such as outdoor condition, heat gain through glass, transmission gain through wall etc. As per the heat load calculated proper selection of outdoor unit and indoor unit was done using Toshiba manual. The schematic of pipe and indoor is displayed considering cost effectiveness. The obtained results were validated by the industry.

Keywords:

R410A, ISHRAE, outdoor unit, indoor unit, cassette, British Thermal Unit, compressor

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CHAPTER 1

1. INTRODUCTION

1.1 Background:

Variable refrigerant flow (VRF), also known as variable refrigerant volume (VRV), is an HVAC technology invented by Daikin Industries, Ltd. in 1982. Like ductless mini splits, VRFs use refrigerant as the cooling and heating medium.

Variable refrigerant flow (VRF) systems vary the flow of refrigerant to indoor units based on demand. This ability to control the amount of refrigerant that is provided to fan coil units located throughout a building makes the VRF technology ideal for applications with varying loads or where zoning is required.

VRF systems are available either as heat pump systems or as heat recovery systems for those applications where simultaneous heating and cooling is required. In addition to providing superior comfort, VRF systems offer design flexibility, energy savings, and cost-effective installation

1.2 VRF Technology:

In a VRF system, multiple indoor fan coil units may be connected to one outdoor unit. The outdoor unit has one or more compressors that are inverter driven, so their speed can be varied by changing the frequency of the power supply to the compressor. As the compressor speed changes, so does the amount of refrigerant deliver by the compressor.

Variable Refrigerant Flow (VRF) system is an air conditioning system which uses refrigerant as a medium to provide zonal cooling and heating. It varies the flow of refrigerant to each room as per the required condition. the compressor used is driven by inverter so that by changing the speed of compressor the flow of refrigerant can be varied hence, the variable flow system. This ability to control the flow of refrigerant makes the VRF system ideal for applications

with varying load or where zonal heating and cooling is desired. VRF systems provide design flexibility, energy savings, and cost-effective installation along with superior comfort.

Each indoor fan coil unit has its own metering device that is controlled by the indoor unit itself, or by the outdoor unit. As each indoor unit sends a demand to the outdoor unit, the outdoor unit delivers the amount of refrigerant needed to meet the individual requirements of each indoor unit.

These features make the VRF system ideally suited for all applications that have part load requirements based on usage or building orientation, as well as applications that require zoning

1.3 Problem Definition:

The traditional air conditioning system used takes up a lot of space and maintenance cost is quite high. moreover, they use of ducts which introduce cooling and heating losses. besides the control over the flow of refrigerant or coolant is not possible as the pump speed cannot be varied. They also have high operation cost.in order to solve these problems we have implemented VRF system considering the required cooling load.

1.4 Project Aim & Objectives:

1.4.1 Aim:

- The main aim is to design and install a Variable refrigerant flow (VRF) system in MTNL building.
- To provide heating ventilation and cooling by providing system which is environmentally friendly.
- To provide cooling and ventilation in economic cost
- To provide consistent comfort to occupants
- To ensure the quite operation of the system
- To design the system such that it provides zonal heating and cooling

1.4.2 Objectives:

- To design energy efficient system
- To provide heating ventilation and cooling by providing system which is environmentally friendly.
- To provide cooling and ventilation in economic cost.
- To provide consistent comfort to occupants.
- To ensure the quiet operation of the system.
- To design the system such that it provides zonal heating and cooling



CHAPTER 2

2. LITERATURE SURVEY

2.1 Variable Refrigerant Flow Systems (GSA journal)

Brian Thornton and Anne Wagner published a journal for the General Service Administration of the USA. This journal gives guidelines for application of VRF system. According to it VRF systems can achieve 30% and higher HVAC energy cost savings relative to minimally code conventional compliant systems, or older inefficient systems. Buildings switching from gas heat to VRF systems offer large energy savings, but because of the price differential between electricity and gas, the utility bill savings will be greater when switching to VRF systems. The best opportunities for VRF systems include buildings with these target characteristics like inefficient HVAC systems and high energy costs, lack of cooling or inadequate cooling capacity, although adding cooling capability or capacity may increase total energy usage despite possible reductions in fan and heating energy usage, new building projects that can take advantage of opportunities to reduce floor-to-floor height, or increase usable floor space by removing mechanical equipment from inside the main building areas, VAV systems with electric reheat or heat pumps with electric back-up heat. Up to a 70% reduction in HVAC energy is possible from a VRF system with exhaust air heat recovery when compared to a VAV system with electric reheat, according to an energy modeling study (Hart and Campbell 2011), significant heating requirements – the Midwest and Northeast are good places to look for opportunities in this regard.

2.2 Installation guide VRF system

It is a manual published by Ingersoll Rand. It gives step by step guide lines for installation of VRF system. Various safety precaution is explained. Guidelines for proper selection of tools and pipe dimeters is given. It explains orientation of outdoor unit and safety measures while

transporting it as per the required tonnage. Various test that need nbe carried out after installation are explained unit.

2.3 Comparative Thermodynamic and economic analysis of conventional HVAC and

VRF system

Emrah` zahi, Aseguil Abusoglu,A. ihsan Kutlar,Oguzhan Dagci carried out an experiment where they did thermodynamic and economic analyses of an existing social and cultural building which has a heating and cooling area of 8852 m² by comparing of a conventional HVAC and a VRF system. A novel contribution is given to the open literature by comparing two systems with actual data measured from the existing system. This study contains insulation, heating and cooling accounts of a building together. In this paper, VRF system is modelled to the existing building for the comparison of the conventional HVAC system. Both systems have been compared in terms of heating and cooling capacity, initial, operation and maintenance costs. It is found that the VRF system is more economic and efficient such that the VRF system is found to have 44% cost profit when compared with the conventional HVAC system.

2.4 A review of HVAC with VRF system

Kartik Patel did a research on VRF system and its energy saving potential in India. According to the study VRF technology is relatively new in India and gained the momentum after 2007. So, this is been relatively new and efficient way to design HVAC system with VRF technology. VRF technology uses smart integrated controls, variable speed drives, refrigerant piping, and heat recovery to provide products with attributes that include high energy efficiency, flexible operation, ease of installation, low noise, zone control, and comfort using all-electric technology. Still efficiency and energy saving depend on many variables which controls heat load of the building. So, energy saving from VRF technology may vary from 10% to 40%

2.5 Design of HVAC with VRF system for a space house in Ahmedabad

Kartik M Patel a PG student designed VRF system for a space house. Various heat load gain, energy efficiency ratio (EER) was calculated. The cost of the project was estimated. Design has been done using ISHRAE standards.

2.6 Developed a new VRF simulation module based on physics in Energy Plus version

With their comparison between measured and simulated results, normalized mean bias errors (NMBEs) were 2.8% and 4.5% for cooling and heating operations. Saving potential of VRV air conditioners could be high as 18 % compared to the energy consumed by split air-conditioning systems when used for appropriate applications. Therefore, the VRV system can be considered as a potential candidate for the installations where the building occupancy and cooling load are regularly varying. Further, Chiller (Central) air-conditioning system can also be considered as a potential candidate as it performs almost efficiently as the VRV system. It consumes around 4 % more energy than VRV system.

The major objective of the research study was to analyses the suitability of VRV air- conditioning system, analyses the actual saving potential and cost effectiveness of VRV air- conditioning system compared to the other available types of air-conditioning systems and access the maintainability of VRV air-conditioning system. (UNIVERSITY OF MORATUWA)

CHAPTER 3

3. TOTAL COSTING

Cost of AIR CONDITIONING						
1	Supplying, Installing, Testing & commissioning of outdoor type of following capacity air cooled 100% inverter compressor based VRV/VRF system using R410A/R407 refrigerant, i/c first fill of refrigerant. The system shall be suitable to operate on 3 phase, 415 V 50 HZ AC power supply and shall comprise of DC Twin Rotary/Scroll compressor, air cooled condensers and its fan with motor, micro-processors controls, control panels, suitable starters, along with internal control and power wiring internal interconnecting refrigerant pipes, charging ports, system single enclosure (the electrical and electronic components assemblies shall be protected with IP - 55 enclosures). Unit shall be complete with suitable safety steel structure COP levels not less than 5.25 at 50% capacities.					
a)	VRF Outdoor Units (28 HP) combination of 14.0 HP X 2Nos	6	Each	577318	Each	3463908.00
2	SITC of Cassette VRF type four directional air flow DX split indoor air conditioning units of the following capacity for mounting inside false ceiling, each comprising of cooling coil, blower with multispeed motor, electronic expansion valve ,supply and return air grill, filter, insulated connection of refrigerant circuit, intake airport for fresher air entry, condensate water drain					

	pump with electronic level sensor complete, suitable to operate from central remote control & installation from ceiling with all required supports, anchor fasteners hardware's, interconnecting refrigerant copper piping, valves, supports etc. including termination at nearest power outlet with copper wire of 3C x 2.5 sq.mm in metallic flexible conduit and interlocking with outdoor units including remote controller. Units shall conform to the detailed specification of the tender document.					
a)	1.6 TR	2	Each	47117	Each	94234.00
b)	2.5 TR	24	Each	52696	Each	1264704.00
c)	3.0 TR	31	Each	59516	Each	1844996.00
3	Supplying & fixing Interconnecting refrigerant copper piping work with supplying and fixing (19 mm thick) closed cell elastomeric nitrile rubber tubular insulation between each set of indoor & outdoor units as per specifications, all piping inside the building shall be properly supported with MS hanger etc. complete as required. The piping shall be laid in masonry shafts, wall, roof/ ceiling, partly in existing pipe well supported at specific intervals with wooden patterns and screwed with anchor fasteners. (The insulation shall be 19 mm thick of NITRILE RUBBER).					
a)	47.625mm OD or 1 7/8" dia	130	Meter	1677	Meter	218010.00
b)	41.275mm OD or 1 5/8" dia	130	Meter	1410	Meter	183300.00

c)	34.925mm OD or 1 3/8" dia	60	Meter	1286	Meter	77160.00
d)	28.575 mm OD or 1 1/8" dia	75	Meter	1019	Meter	76425.00
e)	25.4 mm OD or 1" dia	135	Meter	966	Meter	130410.00
f)	22.225 mm OD or 7/8" dia	150	Meter	841	Meter	126150.00
g)	19.05 mm OD or 3/4" dia	95	Meter	705	Meter	66975.00
h)	15.875 mm OD or 5/8" dia	150	Meter	580	Meter	87000.00
I)	12.7 mm OD or 1/2" dia	130	Meter	501	Meter	65130.00
j)	9.525 mm OD or 3/8" dia	150	Meter	399	Meter	59850.00
k)	6.35 mm OD or 1/4" dia	130	Meter	260	Meter	33800.00
4	SITC of insulated Copper Refrigerant Branch Kit/ Refinet Joint for VRV piping complete as required. The insulation shall be 19 mm thick of NITRILE RUBER.	57	Each	3864	Each	220248.00
5	Supplying, installation, testing and commissioning of heavy gauge UPVC drain Piping for the VRV system fully insulated with 6mm thick NITRILE RUBBER insulation with adequate supports as per specification and instructions of Engineer in charge etc. as required.					
a)	25 mm dia.	90	Meter	144	Meter	12960.00

b)	32 mm dia.	290	Meter	177	Meter	51330.00
c)	40mm dia.	90	Meter	202	Meter	18180.00
d)	50mm dia.	70	Meter	255	Meter	17850.00
6	Supplying, laying and fixing control cum transmission cable between indoor and outdoor units of size 2 core x 2.5 sq.mm XLPE/PVC insulated copper conductor in PVC conduit including accessories like cable glands & Lugs etc. as required.	800	Meter	132	Meter	105600.00
7	Supplying Fabrication of MS frame structure suitable for mounting outdoor VRF unit mesh out of suitable thickness and section i/c cutting, welding and panting with 2 coats of synthetic enamel paint after primer, fixing on wall with anchor fastener etc. complete as required.	1250	Meter	Kg.	Meter	190000.00
	TOTAL COST					8408220.00

Table 1. Total Cost of Project

CHAPTER 4

4. METHODOLOGY:

4.1. Steps of Methodology

The following are steps followed by industries for designing VRF system

- **Site visit of engineer:** the site engineer visits the site and analyze the site and gets the architectural layout.
- **Area measurement:** This involves calculation of area which requires cooling.
- **Heat and cooling load Calculation:** Heating and cooling load are calculated considering outdoor condition, heat gain through wall, ceiling, roof etc. Heat load calculation is a fundamental skill for HVAC designers and consultants. Consider that space cooling is among the highest energy expenses in buildings, especially during the summer. However, to properly size a space cooling system, first we must know the amount of heat that must be removed - this is precisely the purpose of heat load calculation. Heat in buildings can come from internal sources such as electrical appliances, or from external sources such as the sun, heat gain through wall, ceiling, roof. A heat load calculation considers all sources present and determines their total effect.
- **Selection of indoor & outdoor unit, line of piping:** Based on the heat load calculated selection of indoor and outdoor unit is done. As per the selected outdoor and indoor units pipe dimensions for main line and branches is done using Toshiba manual.
- **Layouts & drafting:** The layout of line of piping from outdoor to indoor is created using drafting software like Auto CAD. the layout drawing is a running record of ideas and problems posed as the design evolves. In most cases the layout drawing ultimately

becomes the primary source of information from which detail drawings and assembly drawings are prepared by other draftsman under the guidance of the designer.

- **Purchasing and BOQ:** Purchasing is a business or organization attempting to acquire goods or services to accomplish its goals. Although there are several organizations that attempt to set standards in the purchasing process, processes can vary greatly between organizations. The purchasing department purchase the materials required like steel sheets for ducts, cooper pipes.
- **Material procurement:** Procurement is a term describing the purchasing process for goods and services. In material procurement is the process by which the materials required are selected, ordered, invoiced, paid for and delivered to the site. procurement typically includes expediting, supplier quality, and transportation and logistics
- **Segregation:** it involves systematic sorting of material and storing it using various work place organization technique to save space and time.
supporting is structure used to hang the indoor cassette and branch controller and other components
- **Drain line/Condensate line:** The condensate line is one of the most important components of your HVAC system. Your condensate line, also known as a condensate drain line or condensate drain does several jobs, but none are more critical to the functionality of your appliance than draining excess moisture outside of your home. It is of particular importance during periods of heavy heating or cooling.

As air is heated or cooled inside your HVAC system, humidity is released. This humidity eventually turns into condensation which must have somewhere to go. Enter: the condensate line. Your condensate line is essentially a drain line. It's typically made out of plastic (commonly PVC) or sometimes metal, although plastic is preferable. It connects directly to the HVAC unit then leads outdoors, often through an exterior wall. Its job is to efficiently funnel condensation away from your HVAC unit; sometimes a small pump is

attached to the HVAC system to expedite the process, but most condensate lines utilize gravity

- **Machine hanging & copper piping:** supporting structure is used to hang the indoor cassette and branch header and other machine components. Two copper pipelines are used one is gas line and other is liquid line, which is connected between outdoor and indoor units. The pipes have varying cross-section which is gradually decreasing from outdoor unit to indoor unit
- **Wiring:**
- **Leak detection:** Due to refrigerant leakage, the running time of the system increases continuously. Both suction as well as discharge pressures reduce due to loss of refrigerant. There will be less liquid and more flash gas, which has negative effect on several components of the system.

Following are different method of refrigerant leakage detection:

Visual Inspection, Soap Water Detection, Water Immersion Method, Halide Torch, Dye Interception Method, Electronic Leak Detection, Ultrasonic Leak Detection, Fluorescent Leak Detection, Nitrogen Water Detection, Gas Pressure Detection

- **Insulation:** After determining that there are no leaks in the refrigerant pipes are insulated. Insulation is done around the entire surface of each pipe, including the refrigerant pipes from the indoor unit to the service valves inside the outdoor unit, the branch joints, distribution header, and connection points on each pipe.
- **Vacuum:** In a refrigerant system, only the refrigerant and oil should be circulating. During servicing or after many years of operation, the air may enter the system. The air from the atmosphere that enters the system include oxygen, nitrogen and moisture. These unwanted components will cause Rise in head pressure, Acids are produced in the refrigerant causing electroplating and damage to the motor insulation, Sludge is formed by a combination of oil, acid and moisture in the system

In order to remove all the unwanted moisture and gases from the refrigerant system, a state of near vacuum has to be achieved in which the pressure in the system is forced to go below the atmospheric pressure Commissioning & Testing

- **Commissioning and testing:** The commissioning process of any installation is critical as it provides official certification and confirmation that a piece of equipment is performing as it should. For our VRF systems, the commissioning process begins with a pressure test using nitrogen to find leaks, testing the system at a certain level. It is kept in this condition for a minimum of 24 hours to ensure it can maintain the same pressure level before the nitrogen is allowed to die out. This first section consists of three elements – a leak test, a pressure test and a strength test.
- **Payment by customer.**
- **Hand over to customer.**

CHAPTER 5

5. Theory of VRF System

5.1 Introduction of Air-conditioning System

Air conditioning (often referred to as AC, A/C, or air con) is the process of removing heat and moisture from the interior of an occupied space, to improve the comfort of occupants. Air conditioning can be used in both domestic and commercial environments. This process is most commonly used to achieve a more comfortable interior environment, typically for humans and other animals; however, air conditioning is also used to cool/dehumidify rooms filled with heat-producing electronic devices, such as computer servers, power amplifiers, and even to display and store some delicate products, such as artwork.

Air conditioners often use a fan to distribute the conditioned air to an occupied space such as a building or a car to improve thermal comfort and indoor air quality.

Electric refrigerant-based AC units range from small units that can cool a small bedroom, which can be carried by a single adult, to massive units installed on the roof of office towers that can cool an entire building. The cooling is typically achieved through a refrigeration cycle, but sometimes evaporation or free cooling is used. Air conditioning systems can also be made based on desiccants (chemicals which remove moisture from the air). Some AC systems reject or store heat in subterranean pipes.

In the most general sense, air conditioning can refer to any form of technology that modifies the condition of air (heating, (de-) humidification, cooling, cleaning, ventilation, or air movement).

In common usage, though, "air conditioning" refers to systems which cool air. In construction, a complete system of heating, ventilation, and air conditioning is referred to as HVAC.

5.2 what is VRF system

Variable Refrigerant Flow (VRF) system is an air conditioning system which uses refrigerant as a medium to provide zonal cooling and heating. It varies the flow of refrigerant to each room as per the required condition. the compressor used is driven by inverter so that by changing the speed of compressor the flow of refrigerant can be varied hence, the variable flow system. This ability to control the flow of refrigerant makes the VRF system ideal for applications with varying load or where zonal heating and cooling is desired. VRF systems provide design flexibility, energy savings, and cost-effective installation along with superior comfort.

5.3 Types of VRF system

5.3.1. Heat Pumps system – 2 pipes

VRF heat pump systems commonly known as 2 pipes, permit heating or cooling in all of the indoor units but NOT simultaneous heating and cooling. When the indoor units are in the cooling mode, they act as evaporators; when they are in the heating mode, they act as condensers.



Figure 5-1. Cooling from Outdoor Unit to Different Section

VRF heat pump systems are effectively applied in open plan areas, retail stores, cellular offices and any other area that require cooling or heating during the same operational periods.

5.3.2. Heat Recovery System- 3 pipe

Variable refrigerant flow systems with heat recovery (VRF-HR) capability can operate simultaneously in heating and/or cooling mode, enabling heat to be used rather than rejected as it would be in traditional heat pump systems. Each indoor unit is branched off from the 3 pipes using solenoid box which contains a series of valves. An indoor unit requiring cooling will open its liquid line and suction line valves and act as an evaporator. An indoor unit requiring heating will open its hot gas and liquid line valves and will act as a condenser. Typically, extra heat exchangers in distribution boxes are used to transfer some reject heat from the superheated refrigerant exiting the zone being cooled to the refrigerant that is going to the zone to be heated. This balancing act has the potential to produce significant energy savings. Three pipe heat pump systems are effectively applied in open plan areas, retail stores, cellular offices and any other area that require cooling and heating at the same time.



Figure 5-2. Heating and Cooling at Different Section from Outdoor Unit

5.3.3. VRF Water Cooled

Most commonly used are air-cooled systems, using packaged outdoor condensing units, which via refrigeration pipework connect to a number of indoor units. There are however some limitations, pipework runs, mainly vertical risers (although Samsung can have a vertical rise up to 115meters), plant space and noise. Where these become an issue then water-cooled systems can be used. They operate as the Air-cooled units, but instead of having a built-in air-cooled heat exchanger they utilise a plate heat exchanger, which transfers the energy into a water loop.



Figure 5-3. VRF Water Cooling

This is connected to a cooling tower or dry cooler which transfers the energy/ heat to atmosphere. Due to this process the water cooled VRF systems can be placed internally with no worry about the vertical risers, in much smaller areas, taking up less space and can be attenuated to meet most environmental requirements. These systems are also ideal for building served by an existing landlords condenser water loop

5.4 Components of VRF system

5.4.1 Outdoor unit:

In a VRF system, multiple indoor fan coil units may be connected to one outdoor unit. The outdoor unit has one or more compressors that are inverter driven, so their speed can be varied by changing the frequency of the power supply to the compressor. As the compressor speed changes, so does the amount of refrigerant delivered by the compressor.

Types of outdoor unit:

- Top Discharge ODU.
- Side Discharge ODU.
- Higher Efficiency ODU.
- Medium Normal Range ODU.



Figure 5-4. Outdoor Unit

5.4.2. Indoor unit

The indoor unit of the split air conditioner is a box type housing in which all the important parts of the air conditioner are enclosed. The most common type of the indoor unit is the wall mounted type though other types like ceiling mounted and floor mounted are also used. An indoor unit containing the evaporator coil and blower. Split-system central air conditioning is most popular

type of residential heating and air-conditioning. The indoor unit is often connected to a furnace or heat pump.



Figure 5-5. Indoor Unit

Types of indoor units

1. **4-way cassette type** - Extremely quiet operation. By employing a super-high-stream turbo fan (three-dimensional twisted wing large bore and high efficiency), the wind flow of efficiency has been improved. With the under damping slit mounted near the center of the revolving shaft, the abnormal noise which is unique to DC motors caused by the number of magnetic poles and revolution speed of the motor, is reduced. With a broad range of air supply, it is suitable to be used.

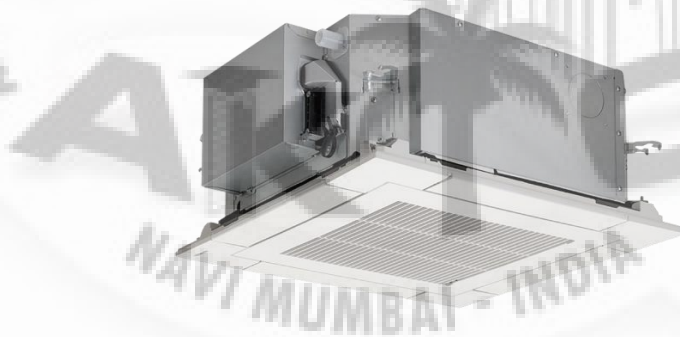


Figure 5-6. 4-way cassette

2. **Compact 4-way cassette type** - Installing the Mini 4 Way Cassette is easy. This compact air conditioning unit can fit into one standard ceiling tile measuring 600 W x 600 D, meaning that alterations are unnecessary. With no extra construction work to carry out, set-up time is reduced, as is the subsequent financial impact on businesses.



Figure 5-7. Compact 4-way cassette

3. **2-way cassette type-** The two-way cassette discharges in two directions. The two way is ceiling mounted and includes its own filter system. The ceiling-cassette indoor units in these duct-free split heat-pump systems provide comfort in large, open spaces. One-way air-flow ceiling-cassette indoor units.

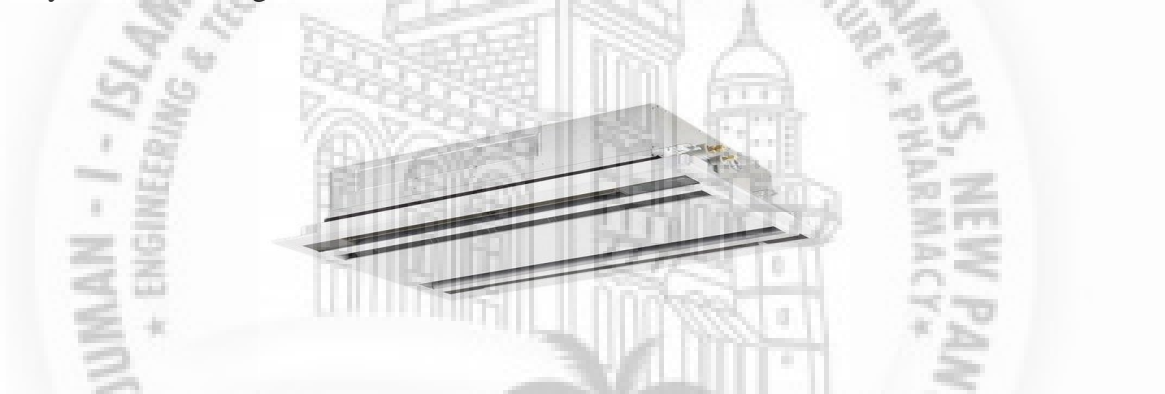


Figure 5-8. 2-way cassette

4. **1-way cassette type-** At a height of only 135mm, the Slim 1Way Cassette is the world's thinnest indoor air-cooling unit. The compact, lightweight design makes installation and maintenance in your space easier than ever. These high-performing units are so subtle that they can easily blend into interiors of all types and styles.



Figure 5-9. 1-way cassette

5. **Concealed duct**, standard type- Type and size of outdoor units and indoor units, and input air flow and external static pressure (ESP) for *ducted* indoor ... Heating and Cooling Equipment *Standard* for Safety and bear the ... Ceiling-*Concealed Ducted* units are designed for air volume against ... Cooling range can be extended from 5°F down to -4°F

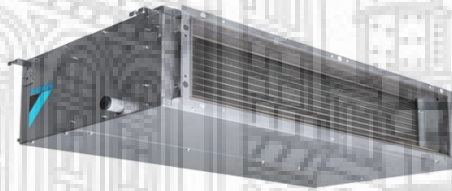


Figure 5-10. Concealed Duct Type

5.4.3 Raffinates (Y-joint):

Raffinates is usually called as Y-joint. Which is used to branching the pipes from outdoor unit to indoor unit. It is made up of copper with insulation cover which may protect the leakage of refringent. It is available in many sizes as per the requirement.

This joint is mainly placed between the indoor AC units & branch to the others. It is always placed parallel to the surface in order to prevent pressure loss.



Figure 5-11. Raffinates (Y-joints)

5.4.4 Copper Pipes:

Copper tubing is most often used for the supply of hot and cold tap water, and as a refrigerant line in HVAC systems. There are two basic types of copper tubing, soft copper and hard copper. Copper tubing is joined using flare connection, compression connection, or solder.

1. Soft Drawn Copper Tubes Coils, Pipes:

Soft drawn, annealed, bending type copper tubes, coils, pipe for various gauge, length, size, surface finish with high quality. Suitable for VRF, VRV, Air-conditioner, Chiller applications.



Figure 5-12. Soft Drawn copper pipe

2. Hard Drawn Copper Pipes:

These type of copper tubes are rigid, hard and stiff. It is not easy to bent and should not be bent. There are three standard weight with different wall thickness for each type. Type K has the thickest wall tubing followed by Type L and Type M.

Type L outer diameters typically starts from 3/8 inch followed by 1/2-inch, 5/8-inch, 3/4-inch, 7/8-inch, 11/8-inch, 13/8-inch, 15/8-inch, 21/8 inch and 25/8 inch.



Figure 5-13. Hard Drawn Copper Pipes

5.4.5 Insulation:

Insulation is to prevent heat transfer between refrigerant and surrounding air. Under cooling mode of VRF system, the optimum insulation thickness varies between 7 and 8 mm for pipe sections of low-pressure gas pipeline and low-pressure liquid pipeline.



Figure 5-14. Insulation

CHAPTER 6

6. HEAT LOAD CALCULATION

6.1 Method of heat load estimation

- Step One

Calculate the area in square feet of the space to be cooled,

- Step Two

Calculate CFM ventilation

CFM ventilation= (area x height x no of air change)/60

CFM person= (no person x CFM/person)

Select the higher of the two as CFM ventilation for calculation

- Step three

Find difference in DB temperature as well as GR/LB of inside and outside

By referring ISHRAE handbook and psychometric chart

- Step four

Calculate sun heat gain

Solar gain through glass (BTU) = area x temp difference x factor (BTU)

Other transmission gain (BTU) = area x temp difference x factor (BTU)

Bypass outside air sensible load (BTU) = CFM ventilation x 0.08 x 1.08 x temperature difference

get factor from ISHRAE handbook table 12

- Step five

Calculate internal sensible heat (BTU)

heat generated by occupants (BTU) = number of people x 245

Heat generated by appliances (BTU) = total equipment watts x 3.4

Heat generated by lights = (BTU) total equipment watts x 3.4

Total heat load (BTU) = solar gain through glass (BTU)+ other transmission gain (BTU)+ bypass outside air sensible load (BTU)+ internal sensible heat (BTU)

Leak loss (BTU) = 5% total heat load

Safety factor (BTU) = 5% total heat load

Total room sensible heat = Total heat load (BTU)+ Leak loss (BTU) + Safety factor (BTU)

- Step Six

Calculate outside air latent load (BTU) =CFM ventilation x G difference x bypass factor x 0.68

Internal latent heat (BTU) =no of people x factor

Get factor from ISHRAE handbook table 12

Subtotal (BTU) = outside air latent load (BTU) + Internal latent heat (BTU)

Safety factor (BTU) = 5% sub total

Total room latent heat = Subtotal (BTU) + Safety factor (BTU)

Room total heat = Total room sensible heat+ Total room latent heat

- Step seven

Outside air heat = CFM ventilation x G. Difference x (1-B.F.) x factor

Heat gain safety @ 3% = 3% Room total heat

Grand total heat (BTU) = Room total heat+ Outside air heat+ Heat gain safety @ 3%

Grand total heat (TONS) = Grand total heat (BTU)/12000

- Step eight

Sensible heat factor = Total room sensible heat/ Room total heat

Selected ADP= (ISHRAE table 15)

Dehumidified rise = (1-B.F.) (Temp difference – ADP)

Dehumidified air CFM = Total room sensible heat/ (1.08 x Dehumidified rise)

Tons as per CFM = Dehumidified air CFM/400

- Step nine

Check results

Grand total heat (BTU/HR/SQFT) = Grand total heat/area

Room sensible heat (BTU/HR/SQFT) = Room sensible heat/area

SQFT/ person = area/no of person

TONS/person = Grand total heat (TONS)/ no of person

Dehumidified CFM/ TONS = Dehumidified air CFM/ Grand total heat (TONS)

Area/TONS = area/ Grand total heat (TONS)

6.2 Heat load estimation

The heat load for each room on the office floor is calculated using the method as shown above and is displayed in the tables below

DESIGN CONDITION, DESIGN DETAIL:

❖ Design location:

- Location: Office building, sector-16, Vashi, Navi Mumbai, Maharashtra 400703.
- Latitude: 18.54° North.

❖ Design Data:

SR. NO.	NAME OF ROOM	AREA (SQFT)	HEIGHT (FOOT)	LIQHTING (W/SQFT)	NO. OF AIR CHANGE	CFM/VENTILATION
1.	STAFF AREA-1	1400	11	1.5	2	513
2.	DCIT-1	200	11	1.5	2	73
3.	DCIT-2	200	11	1.5	2	73
4.	ITO-1	190	11	1.5	2	70
5.	ITO-2	190	11	1.5	2	70
6.	ITO-3	190	11	1.5	2	70
7.	ITO-4	190	11	1.5	2	70
8.	STAFF AREA-2	1200	11	1.5	2	440
9.	CIT A	270	11	1.5	2	99
10.	AO AND PS (A)	240	11	1.5	2	88

11.	JCTI-1	290	11	1.5	2	106
12.	ADDL JCTI-1	270	11	1.5	2	99
13.	CIT (B)	270	11	1.5	2	99
14.	AO AND PS (B)	210	11	1.5	2	77

Table 2. CFM/Ventilation Calculation on the Basis of Area

Calculate CFM ventilation:

$$\text{CFM Ventilation} = \frac{(\text{Area} \times \text{Height of the area} \times \text{Lighting} \times \text{No. of air change})}{60}$$

Where,

CFM= Air flow in cubic feet per minute

SR NO.	NAME OF ROOM	CFM /PERSON	NO. OF PERSON	CFM/VENTILATION
1.	STAFF AREA-1	10	30	300
2.	DCIT-1	10	07	70
3.	DCIT-2	10	07	70
4.	ITO-1	10	06	60
5.	ITO-2	10	06	60
6.	ITO-3	10	06	60
7.	ITO-4	10	06	60
8.	STAFF AREA-2	10	30	300
9.	CIT A	10	10	100
10.	AO AND PS (A)	10	06	60
11.	JCTI-1	10	10	100
12.	ADDL JCTI-1	10	10	100
13.	CIT (B)	10	10	100
14.	AO AND PS (B)	10	02	20

Table 3. CFM/Ventilation Calculation on the Basis of No. of Persons

$$\text{CFM Ventilation} = \text{CFM/person} \times \text{No. of person}$$

❖ Design Condition:

PARAMETER	D.B.(F°)	W.B.(F°)	%RH	GR/LB
OUTSIDE	100	83	60	146
INSIDE	75	-	50	64
DIFFERENCE	25	-	-	82

Table 4.Design Condition

6.2.1 STAFF AREA-1❖ SENSIBLE HEAT GAIN:

SOLAR GAIN- GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	11	0.56	0
SOUTH	0	11	0.56	0
EAST	19	11	0.56	117
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	20	0.34	0
SOUTH	0	36	0.34	0
EAST	52	22	0.34	390
WEST	363	36	0.34	4443
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	1400	51	0.15	0

OTHER TRANSMISSION GAIN				
AGLS	AREA	T.DIFF.	FACTOR	BTU
AGLS	19	25	1.13	537

PART	1023	20	0.34	6956
CEIL	1400	20	0.34	9520
FLOR	1400	20	0.34	9520

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
513	25	0.08	1.08	1108

INTERNAL SENSIBLE LOAD				
PEOPLE	30	245		7350
APPL.	5000	3.4		17000
LIGHTS	2100	3.4	1.25	8925
FOOD	0	60		0
SUB TOTAL				65866

LEAK LOSS +SAFETY FACTOR=5%	3293
ROOM SENSIBLE HEAT	72452

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
513	82	0.08	0.68	2288

INTERNAL LATENT LOAD			
PEOPLE	30	205	6150

SUB TOTAL	8438
SAFETY FACTOR=5%	422
ROOM LATENT HEAT	8860
ROOM TOTAL HEAT	81312

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	513	25	0.92	1.08	12743

LATENT	513	82	0.92	0.68	26316
SUB TOTAL					39059
TOTAL					120371
HEAT GAIN SAFETY FACTOR @ 3%					3611
GRAND TOTAL HEAT	(TONS)	10.3	123982		

SENSIBLE HEAT FACTOR	0.89
SELECTED A.D.P.	54
DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	3354
TONS AS PER Cfm	8.38

GRAND TOTAL HEAT (BTU/HR/SQFT.)	92
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	51.75
SQFT/PERSON	46.67
TONS PER SQFT	0.01
CFM PER SQFT	2.39
TONS/PERSON	0.34
DEHUMIDIFIED CFM/TON	325.63
AREA PER TON	135.92

Table 5. Calculation of staff Area-1

6.2.2. DCIT-1

❖ SENSIBLE HEAT GAIN:

SOLAR GAIN-GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	11	0.56	0
SOUTH	0	11	0.56	0
EAST	0	11	0.56	0
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
NORTH	0	20	0.34	0
SOUTH	0	36	0.34	0
EAST	0	22	0.34	0
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	200	51	0.15×0	0

OTHER TRANSMISSION GAIN				
AGLS	0	25	1.13	0
PART	176	20	0.34	1197
CEIL	200	20	0.34	1360
FLOR	200	20	0.34	1360

BYPASS O.A. SENSIBLE LOAD					
	CFM	T.DIFF.	BYPASS	FACTOR	BTU
	73	25	0.08	1.08	158

INTERNAL SENSIBLE LOAD				
PEOPLE	7	245		1715
APPL.	250	3.4		850
LIGHTS	300	3.4	1.25	1275
FOOD	0	60		0
SUB TOTAL				7915

LEAK LOSS +SAFETY FACTOR=5%	396
ROOM SENSIBLE HEAT	8707

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
73	82	0.08	0.68	326

INTERNAL LATENT LOAD			
PEOPLE	7	205	1435

SUB TOTAL	1761
SAFETY FACTOR=5%	88
ROOM LATENT HEAT	1849
ROOM TOTAL HEAT	10556

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	73	25	0.92	1.08	1813
LATENT	73	82	0.92	0.68	3745
SUB TOTAL					5558
TOTAL					16114
HEAT GAIN SAFETY FACTOR @ 3%					483
GRAND TOTAL HEAT			(TONS)	1.38	16597

SENSIBLE HEAT FACTOR	0.82
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	403
TONS AS PER Cfm	1.0

GRAND TOTAL HEAT (BTU/HR/SQFT.)	82.98
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	43.53
SQFT/PERSON	28.57
TONS PER SQFT	0.01
CFM PER SQFT	2.01
TONS/PERSON	0.19
DEHUMIDIFIED CFM/TON	292.10
AREA PER TON	144.92

Table 6. Calculation of DCIT-1

6.2.3. DCIT-2❖ **SENSIBLE HEAT GAIN:**

SOLAR GAIN-GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	11	0.56	0
SOUTH	0	11	0.56	0
EAST	0	11	0.56	0
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
NORTH	0	20	0.34	0
SOUTH	0	36	0.34	0
EAST	0	22	0.34	0
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	200	51	0.15×0	0

OTHER TRANSMISSION GAIN				
AGLS	0	25	1.13	0
PART	176	20	0.34	1197
CEIL	200	20	0.34	1360
FLOR	200	20	0.34	1360

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
73	25	0.08	1.08	158

INTERNAL SENSIBLE LOAD

PEOPLE	7	245		1715
APPL.	250	3.4		850
LIGHTS	300	3.4	1.25	1275
FOOD	0	60		0
SUB TOTAL				7915

LEAK LOSS +SAFETY FACTOR=5%	396
ROOM SENSIBLE HEAT	8707

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
73	82	0.08	0.68	326

INTERNAL LATENT LOAD			
PEOPLE	7	205	1435

SUB TOTAL	1761
SAFETY FACTOR=5%	88
ROOM LATENT HEAT	1849
ROOM TOTAL HEAT	10556

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	73	25	0.92	1.08	1813
LATENT	73	82	0.92	0.68	3745
SUB TOTAL					5558
TOTAL					16114
HEAT GAIN SAFETY FACTOR @ 3%				483	
GRAND TOTAL HEAT			(TONS)	1.38	16597

SENSIBLE HEAT FACTOR	0.82
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20

DEHUMIDIFIED AIR Cfm	403
TONS AS PER Cfm	1.0
GRAND TOTAL HEAT (BTU/HR/SQFT.)	82.98
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	43.53
SQFT/PERSON	28.57
TONS PER SQFT	0.01
CFM PER SQFT	2.01
TONS/PERSON	0.19
DEHUMIDIFIED CFM/TON	292.10
AREA PER TON	144.92

Table 7. Calculation of DCIT-2

6.2.4. ITO - 1

- ❖ SENSIBLE HEAT GAIN:
SUN GAIN:

SOLAR GAIN- SOLAR				
DIRTECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	44	11	0.56	271
SOUTH	0	11	0.56	0
EAST	0	11	0.56	0
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
DIRTECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	78	20	0.34	530
SOUTH	0	36	0.34	0
EAST	0	22	0.34	0
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0

ROOF	190	51	0.15×0	0
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OTHER TRANSMISSION GAIN				
AGLS	44	25	1.13	1243
PART	369	20	0.34	2509
CEIL	190	20	0.34	1292
FLOR	190	20	0.34	1292

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
70	25	0.08	1.08	151

INTERNAL SENSIBLE LOAD				
PEOPLE	6	245		1470
APPL.	250	3.4		850
LIGHTS	285	3.4	1.25	1211
FOOD	0	60		0
SUB TOTAL				10819

LEAK LOSS +SAFETY FACTOR=5%	541
ROOM SENSIBLE HEAT	11901

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
70	82	0.08	0.68	312

INTERNAL LATENT LOAD			
PEOPLE	6	205	1230

SUB TOTAL	1542
SAFETY FACTOR=5%	77
ROOM LATENT HEAT	1619
ROOM TOTAL HEAT	13520

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	70	25	0.92	1.08	1739
LATENT	70	82	0.92	0.68	3591
SUB TOTAL	5330				
TOTAL	18850				
HEAT GAIN SAFETY FACTOR @ 3%					566
GRAND TOTAL HEAT			(TONS)	1.6	19416

SENSIBLE HEAT FACTOR	0.88
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	550
TONS AS PER Cfm	1.37

GRAND TOTAL HEAT (BTU/HR/SQFT.)	102.18
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	62.63
SQFT/PERSON	31.67
TONS PER SQFT	0.01
CFM PER SQFT	2.89
TONS/PERSON	0.27
DEHUMIDIFIED CFM/TON	343.75
AREA PER TON	118.75

Table 8. Calculation of ITO-1

6.2.5. ITO- 2

- ❖ SENSIBLE HEAT GAIN:
SUN GAIN:

SOLAR GAIN- GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	42	11	0.56	259
SOUTH	0	11	0.56	0
EAST	0	11	0.56	0
WEST	0	165	0.56	0

N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
NORTH	81	20	0.34	551
SOUTH	0	36	0.34	0
EAST	0	22	0.34	0
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	190	51	0.15×0	0

OTHER TRANSMISSION GAIN				
AGLS	42	25	1.13	1187
PART	184	20	0.34	1251
CEIL	190	20	0.34	1292
FLOR	190	20	0.34×0	0

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
70	25	0.08	1.08	151

INTERNAL SENSIBLE LOAD				
PEOPLE	6	245		1470
APPL.	250	3.4		850
LIGHTS	285	3.4	1.25	1211
FOOD	0	60		0
SUB TOTAL				8222

LEAK LOSS +SAFETY FACTOR=5%	411
ROOM SENSIBLE HEAT	9044

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
70	82	0.08	0.68	312

INTERNAL LATENT LOAD			
PEOPLE	6	205	1230

SUB TOTAL	1542
SAFETY FACTOR=5%	77
ROOM LATENT HEAT	1619
ROOM TOTAL HEAT	10663

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	70	25	0.92	1.08	1739
LATENT	70	82	0.92	0.68	3590
SUB TOTAL					5329
TOTAL					15992
HEAT GAIN SAFETY FACTOR @ 3%					480
GRAND TOTAL HEAT			(TONS)	1.4	16472

SENSIBLE HEAT FACTOR	0.84
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	418
TONS AS PER Cfm	1.04

GRAND TOTAL HEAT (BTU/HR/SQFT.)	86.69
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	47.6
SQFT/PERSON	31.67
TONS PER SQFT	0.01
CFM PER SQFT	2.2
TONS/PERSON	0.23
DEHUMIDIFIED CFM/TON	299
AREA PER TON	135.71

Table 9. Calculation of ITO-2

6.2.6. ITO- 3:❖ SENSIBLE HEAT GAIN:

SOLAR GAIN- GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	39	11	0.56	240
SOUTH	0	11	0.56	0
EAST	57	11	0.56	351
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
NORTH	81	20	0.34	551
SOUTH	0	36	0.34	0
EAST	0	22	0.34	0
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	1400	51	0.15×0	0

OTHER TRANSMISSION GAIN				
AGLS	96	25	1.13	2712
PART	184	20	0.34	1251
CEIL	190	20	0.34	1292
FLOR	190	20	0.34×0	0

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
70	25	0.08	1.08	151

INTERNAL SENSIBLE LOAD				
PEOPLE	6	245		1470
APPL.	250	3.4		850
LIGHTS	285	3.4	1.25	1211
FOOD	0	60		0
SUB TOTAL				10079

LEAK LOSS +SAFETY FACTOR=5%	504
ROOM SENSIBLE HEAT	11087

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
70	82	0.08	0.68	312

INTERNAL LATENT LOAD			
PEOPLE	6	205	1230

SUB TOTAL	1542
SAFETY FACTOR=5%	77
ROOM LATENT HEAT	1619
ROOM TOTAL HEAT	12706

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	70	25	0.92	1.08	1739
LATENT	70	82	0.92	0.68	3591
SUB TOTAL	5330				
TOTAL	18036				
HEAT GAIN SAFETY FACTOR @ 3%				541	
GRAND TOTAL HEAT			(TONS)	1.5	18577

SENSIBLE HEAT FACTOR	0.87
SELECTED A.D.P.	52

DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	513
TONS AS PER Cfm	1.3
GRAND TOTAL HEAT (BTU/HR/SQFT.)	97.77
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	58.35
SQFT/PERSON	31.67
TONS PER SQFT	0.01
CFM PER SQFT	2.7
TONS/PERSON	0.25
DEHUMIDIFIED CFM/TON	342
AREA PER TON	125.60

Table 10. Calculation of ITO-3

6.2.7. ITO-4:

❖ SENSIBLE HEAT GAIN:

SOLAR GAIN- GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	39	11	0.56	240
SOUTH	0	11	0.56	0
EAST	32	11	0.56	197
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	92	20	0.34	626
SOUTH	0	36	0.34	0
EAST	160	22	0.34	1197
WEST	363	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0

ROOF	1400	51	0.15	0
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OTHER TRANSMISSION GAIN				
AGLS	71	25	1.13	2006
PART	0	20	0.34	0
CEIL	190	20	0.34	1292
FLOR	190	20	0.34	1292

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
70	25	0.08	1.08	151

INTERNAL SENSIBLE LOAD				
PEOPLE	6	245		1470
APPL.	250	3.4		850
LIGHTS	285	3.4	1.25	1211
FOOD	0	60		0
SUB TOTAL				10532

LEAK LOSS +SAFETY FACTOR=5%	527
ROOM SENSIBLE HEAT	11586

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
70	82	0.08	0.68	312

INTERNAL LATENT LOAD			
PEOPLE	6	205	1230

SUB TOTAL	1542
SAFETY FACTOR=5%	77
ROOM LATENT HEAT	1619
ROOM TOTAL HEAT	13205

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	70	25	0.92	1.08	1739
LATENT	70	82	0.92	0.68	3591
SUB TOTAL					5330
TOTAL					18535
HEAT GAIN SAFETY FACTOR @ 3%					556
GRAND TOTAL HEAT			(TONS)	1.6	19091

SENSIBLE HEAT FACTOR	0.87
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	21
DEHUMIDIFIED AIR Cfm	511
TONS AS PER Cfm	1.27

GRAND TOTAL HEAT (BTU/HR/SQFT.)	100.47
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	61
SQFT/PERSON	31.67
TONS PER SQFT	0.01
CFM PER SQFT	2.68
TONS/PERSON	0.26
DEHUMIDIFIED CFM/TON	319.37
AREA PER TON	118.75

Table 11. Calculation of ITO-4

6.2.8. STAFF AREA-2:

❖ SENSIBLE HEAT GAIN:

SOLAR GAIN- GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	141	11	0.56	869
SOUTH	0	11	0.56	0
EAST	0	11	0.56	0
WEST	0	165	0.56	0
N-E	0	11	0.56	0

N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
NORTH	112	20	0.34	762
SOUTH	0	36	0.34	0
EAST	0	22	0.34	0
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	1200	51	0.15×0	0

OTHER TRANSMISSION GAIN				
AGLS	141	25	1.13	3983
PART	1221	20	0.34	8303
CEIL	1200	20	0.34	8160
FLOR	1200	20	0.34	8160

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
440	25	0.08	1.08	1064

INTERNAL SENSIBLE LOAD				
PEOPLE	30	245		7350
APPL.	5000	3.4		17000
LIGHTS	1800	3.4	1.25	7650
FOOD	0	60		0
SUB TOTAL				63301

LEAK LOSS +SAFETY FACTOR=5%	3165
ROOM SENSIBLE HEAT	69631

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
440	82	0.08	0.68	1963

INTERNAL LATENT LOAD			
PEOPLE	30	205	6150

SUB TOTAL	8113
SAFETY FACTOR=5%	406
ROOM LATENT HEAT	8519
ROOM TOTAL HEAT	78150

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
SENSIBLE	440	25	0.92	1.08	10930
LATENT	440	82	0.92	0.68	22572
SUB TOTAL					33502
TOTAL					111652
HEAT GAIN SAFETY FACTOR @ 3%					3350
GRAND TOTAL HEAT			(TONS)	9.58	115002

SENSIBLE HEAT FACTOR	0.89
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	3224
TONS AS PER Cfm	8.06

GRAND TOTAL HEAT (BTU/HR/SQFT.)	95.83
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	58.02
SQFT/PERSON	40
TONS PER SQFT	0.01
CFM PER SQFT	2.68
TONS/PERSON	0.32
DEHUMIDIFIED CFM/TON	336.53
AREA PER TON	125.26

Table 12. Calculation of Staff Area-2

6.2.9. CIT-A:❖ SENSIBLE HEAT GAIN:

SOLAR GAIN- GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	26	11	0.56	160
SOUTH	0	11	0.56	0
EAST	51	11	0.56	315
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
NORTH	130	20	0.34	884
SOUTH	0	36	0.34	0
EAST	181	22	0.34	1354
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	270	51	0.15×0	0

OTHER TRANSMISSION GAIN				
AGLS	77	25	1.13	2175
PART	147	20	0.34	1000
CEIL	270	20	0.34	1836
FLOR	270	20	0.34	1836

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
100	25	0.08	1.08	216

INTERNAL SENSIBLE LOAD				
PEOPLE	10	245		2450
APPL.	250	3.4		850
LIGHTS	405	3.4	1.25	1721
FOOD	0	60		0
SUB TOTAL				14797

LEAK LOSS +SAFETY FACTOR=5%	740
ROOM SENSIBLE HEAT	16277

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
100	82	0.08	0.68	446

INTERNAL LATENT LOAD			
PEOPLE	10	205	2050

SUB TOTAL	2496
SAFETY FACTOR=5%	125
ROOM LATENT HEAT	2621
ROOM TOTAL HEAT	18898

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	100	25	0.92	1.08	2484
LATENT	100	82	0.92	0.68	5130
SUB TOTAL					7614
TOTAL					26512
HEAT GAIN SAFETY FACTOR @ 3%					795
GRAND TOTAL HEAT			(TONS)	2.3	27307

SENSIBLE HEAT FACTOR	0.86
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20

DEHUMIDIFIED AIR Cfm	754
TONS AS PER Cfm	1.88

GRAND TOTAL HEAT (BTU/HR/SQFT.)	101.13
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	60.28
SQFT/PERSON	27
TONS PER SQFT	0.01
CFM PER SQFT	2.79
TONS/PERSON	0.23
DEHUMIDIFIED CFM/TON	327.82
AREA PER TON	117.39

Table 13. Calculation of CIT-A

6.2.10. AO & PS (A):

❖ SENSIBLE HEAT GAIN:

SOLAR GAIN- GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	11	0.56	0
SOUTH	0	11	0.56	0
EAST	51	11	0.56	314
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	20	0.34	0
SOUTH	0	36	0.34	0
EAST	153	22	0.34	1144
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	240	51	0.15×0	0

OTHER TRANSMISSION GAIN				
AGLS	51	25	1.13	1441
PART	131	20	0.34	891
CEIL	240	20	0.34	1632
FLOR	240	20	0.34	1632

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
88	25	0.08	1.08	190

INTERNAL SENSIBLE LOAD				
PEOPLE	6	245		1470
APPL.	500	3.4		1700
LIGHTS	360	3.4	1.25	1530
FOOD	0	60		0
SUB TOTAL				11944

LEAK LOSS +SAFETY FACTOR=5%	597
ROOM SENSIBLE HEAT	13138

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
88	82	0.08	0.68	393

INTERNAL LATENT LOAD				
PEOPLE	6	205		1230

SUB TOTAL	1623
SAFETY FACTOR=5%	81
ROOM LATENT HEAT	1704
ROOM TOTAL HEAT	14842

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	88	25	0.92	1.08	2186
LATENT	88	82	0.92	0.68	4514
SUB TOTAL					6700
TOTAL					21542
HEAT GAIN SAFETY FACTOR @ 3%					646
GRAND TOTAL HEAT			(TONS)	1.85	22188

SENSIBLE HEAT FACTOR	0.88
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	608
TONS AS PER Cfm	1.52

GRAND TOTAL HEAT (BTU/HR/SQFT.)	92.45
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	54.74
SQFT/PERSON	40
TONS PER SQFT	0.01
CFM PER SQFT	2.53
TONS/PERSON	0.30
DEHUMIDIFIED CFM/TON	328.64
AREA PER TON	129.72

Table 14. Calculation of AO&PO(A)

6.2.11. JCTI-1:

❖ SENSIBLE HEAT GAIN:

SOLAR GAIN-GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	11	0.56	0
SOUTH	30	11	0.56	185
EAST	51	11	0.56	314
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0

S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
NORTH	0	20	0.34	0
SOUTH	161	36	0.34	1971
EAST	144	22	0.34	1077
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	200	51	0.15×0	0

OTHER TRANSMISSION GAIN				
AGLS	82	25	1.13	2317
PART	197	20	0.34	1340
CEIL	290	20	0.34	1972
FLOR	290	20	0.34	1972

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
106	25	0.08	1.08	229

INTERNAL SENSIBLE LOAD				
PEOPLE	10	245		2450
APPL.	250	3.4		850
LIGHTS	435	3.4	1.25	1849
FOOD	0	60		0
SUB TOTAL				16526

LEAK LOSS +SAFETY FACTOR=5%	826
ROOM SENSIBLE HEAT	18178

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
106	82	0.08	0.68	473

INTERNAL LATENT LOAD			
PEOPLE	10	205	2050

SUB TOTAL	2523
SAFETY FACTOR=5%	126
ROOM LATENT HEAT	2649
ROOM TOTAL HEAT	20827

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	106	25	0.92	1.08	2633
LATENT	106	82	0.92	0.68	5438
SUB TOTAL					8071
TOTAL					28898
HEAT GAIN SAFETY FACTOR @ 3%					867
GRAND TOTAL HEAT			(TONS)	2.48	29765

SENSIBLE HEAT FACTOR	0.87
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	842
TONS AS PER Cfm	2.1

GRAND TOTAL HEAT (BTU/HR/SQFT.)	102.63
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	62.68
SQFT/PERSON	29
TONS PER SQFT	0.01
CFM PER SQFT	2.90
TONS/PERSON	0.24
DEHUMIDIFIED CFM/TON	339.51
AREA PER TON	116.93

Table 15. Calculation of JCIT-1

6.2.12. ADDL JCTI-1:❖ **SENSIBLE HEAT GAIN:**

SOLAR GAIN-GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	11	0.56	0
SOUTH	38	11	0.56	234
EAST	0	11	0.56	0
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	20	0.34	0
SOUTH	126	36	0.34	1542
EAST	0	22	0.34	0
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	270	51	0.15×0	0

OTHER TRANSMISSION GAIN				
TYPE	AREA	T.DIFF.	FACTOR	BTU
AGLS	38	25	1.13	1074
PART	197	20	0.34	1340
CEIL	270	20	0.34	1836
FLOR	270	20	0.34	1836

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
100	25	0.08	1.08	216

INTERNAL SENSIBLE LOAD				
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PEOPLE	10	245		2450
APPL.	250	3.4		850
LIGHTS	405	3.4	1.25	1721
FOOD	0	60		0
SUB TOTAL				13109

LEAK LOSS +SAFETY FACTOR=5%	655
ROOM SENSIBLE HEAT	14419

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
100	82	0.08	0.68	446

INTERNAL LATENT LOAD			
PEOPLE	10	205	2050

SUB TOTAL	2496
SAFETY FACTOR=5%	125
ROOM LATENT HEAT	2621
ROOM TOTAL HEAT	17040

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	100	25	0.92	1.08	2484
LATENT	100	82	0.92	0.68	5130
SUB TOTAL					7614
TOTAL					24654
HEAT GAIN SAFETY FACTOR @ 3%					740
GRAND TOTAL HEAT			(TONS)	2.1	25394

SENSIBLE HEAT FACTOR	0.84
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	668

TONS AS PER Cfm	1.67
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GRAND TOTAL HEAT (BTU/HR/SQFT.)	94.05
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	53.40
SQFT/PERSON	27
TONS PER SQFT	0.01
CFM PER SQFT	2.47
TONS/PERSON	0.21
DEHUMIDIFIED CFM/TON	318.095
AREA PER TON	128.57

Table 16. Calculation of ADDL JCIT-1

6.2.13. CIT-B

❖ SENSIBLE HEAT GAIN:

SOLAR GAIN-GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	11	0.56	0
SOUTH	34	11	0.56	209
EAST	0	11	0.56	0
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0
S-W	0	113	0.56	0

SOLAR & TRANSMISSION GAIN -WALL				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	20	0.34	0
SOUTH	153	36	0.34	1873
EAST	0	22	0.34	0
WEST	79	36	0.34	967
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	270	51	0.15×0	0

OTHER TRANSMISSION GAIN				
AGLS	34	25	1.13	961
PART	281	20	0.34	1911
CEIL	270	20	0.34	1836
FLOR	270	20	0.34	1836

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
100	25	0.08	1.08	216

INTERNAL SENSIBLE LOAD				
PEOPLE	10	245		2450
APPL.	250	3.4		850
LIGHTS	405	3.4	1.25	1721
FOOD	0	60		0
SUB TOTAL				14830

LEAK LOSS +SAFETY FACTOR=5%	741
ROOM SENSIBLE HEAT	16312

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD				
CFM	G. DIFF	BYPASS	FACTOR	BTU
100	82	0.08	0.68	446

INTERNAL LATENT LOAD				
PEOPLE	10	205		2050

SUB TOTAL	2496
SAFETY FACTOR=5%	125
ROOM LATENT HEAT	2621
ROOM TOTAL HEAT	18933

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	100	25	0.92	1.08	2484
LATENT	100	82	0.92	0.68	5130
SUB TOTAL					7614
TOTAL					26550
HEAT GAIN SAFETY FACTOR @ 3%				796	
GRAND TOTAL HEAT			(TONS)	2.3	27346

SENSIBLE HEAT FACTOR	0.86
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	755
TONS AS PER Cfm	1.9

GRAND TOTAL HEAT (BTU/HR/SQFT.)	101.29
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	60.43
SQFT/PERSON	27
TONS PER SQFT	0.01
CFM PER SQFT	2.76
TONS/PERSON	0.23
DEHUMIDIFIED CFM/TON	328.26
AREA PER TON	117.39

Table 17. Calculation of CIT-B

6.2.14. AO & PS (B):

❖ SENSIBLE HEAT GAIN:

SOLAR GAIN-GLASS				
DIRECTION	AREA	T.DIFF.	FACTOR	BTU
NORTH	0	11	0.56	0
SOUTH	0	11	0.56	0
EAST	0	11	0.56	0
WEST	0	165	0.56	0
N-E	0	11	0.56	0
N-W	0	118	0.56	0
S-E	0	11	0.56	0

S-W	0	113	0.56	0
-----	---	-----	------	---

SOLAR & TRANSMISSION GAIN -WALL				
NORTH	0	20	0.34	0
SOUTH	0	36	0.34	0
EAST	0	22	0.34	0
WEST	0	36	0.34	0
N-E	0	17	0.34	0
N-W	0	13	0.34	0
S-E	0	25	0.34	0
S-W	0	21	0.34	0
ROOF	210	51	0.15×0	0

OTHER TRANSMISSION GAIN				
AGLS	0	25	1.13	0
PART	204	20	0.34	1387
CEIL	210	20	0.34	1428
FLOR	210	20	0.34	1428

BYPASS O.A. SENSIBLE LOAD				
CFM	T.DIFF.	BYPASS	FACTOR	BTU
77	25	0.08	1.08	166

INTERNAL SENSIBLE LOAD				
PEOPLE	2	245		490
APPL.	500	3.4		1700
LIGHTS	315	3.4	1.25	1339
FOOD	0	60		0
SUB TOTAL				7938

LEAK LOSS +SAFETY FACTOR=5%	397
ROOM SENSIBLE HEAT	8732

❖ LATENT HEAT:

BYPASS OUTSIDE AIR LATENT LOAD

CFM	G. DIFF	BYPASS	FACTOR	BTU
77	82	0.08	0.68	343

INTERNAL LATENT LOAD			
PEOPLE	2	205	410

SUB TOTAL	753
SAFETY FACTOR=5%	38
ROOM LATENT HEAT	791
ROOM TOTAL HEAT	9523

❖ GRAND TOTAL HEAT:

OUTSIDE AIR HEAT					
	CFM	G. DIFF	1-B.F.	FACTOR	BTU
SENSIBLE	77	25	0.92	1.08	1913
LATENT	77	82	0.92	0.68	3950
SUB TOTAL					5863
TOTAL					15386
HEAT GAIN SAFETY FACTOR @ 3%					462
GRAND TOTAL HEAT			(TONS)	1.32	15848

SENSIBLE HEAT FACTOR	0.92
SELECTED A.D.P.	52
DEHUMIDIFIED RISE	20
DEHUMIDIFIED AIR Cfm	404
TONS AS PER Cfm	1.01

GRAND TOTAL HEAT (BTU/HR/SQFT.)	75.47
ROOM SENSIBLE HEAT (BTU/HR/SQFT.)	41.58
SQFT/PERSON	105
TONS PER SQFT	0.01
CFM PER SQFT	1.92
TONS/PERSON	0.66
DEHUMIDIFIED CFM/TON	306.06
AREA PER TON	159.09

Table 18. Calculation of AO&PS(B)

6.3. Summary:

SUBJECT: HEAT LOAD SUMMARY SHEET										
PROJECT:		INCOME TAX OFFICE GROUND FLOOR								
SR.	DISCRIPTION	Area	Occupancy	WATTS	Fresh air	APPL.	Dehumidified air	Tonnage	Cfm/HP	Tonnage
		Sq. Ft.	Nos.	Sq. Ft.	CFM	WATTS.		REQ. (TR)		HP
1	STAFF AREA - 1	1400	30	1.5	513	5000	3354	10.3	13.41	12.4
2	DCIT - 1	200	7	1.5	73	250	403	1.38	1.61	1.66
3	DCIT - 2	200	7	1.5	73	250	403	1.38	1.61	1.66
4	ITO - 1	190	6	1.5	70	250	550	1.6	2.2	1.92
5	ITO - 2	190	6	1.5	70	250	418	1.4	1.67	1.68
6	ITO - 3	190	6	1.5	70	250	513	1.5	2.05	1.8
7	ITO - 4	190	6	1.5	70	250	511	1.6	2.04	1.92
8	STAFF AREA - 2	1200	30	1.5	440	5000	3224	9.58	12.89	11.54
9	CIT A	270	10	1.5	99	250	754	2.3	3.01	2.77
10	AO AND PSA	240	6	1.5	88	500	608	1.85	2.43	2.22
11	JCTI -1	290	10	1.5	106	250	842	2.48	3.36	2.98
12	ADDL JCTI - 1	270	10	1.5	99	250	668	2.1	2.67	2.53
13	CIT (B)	270	10	1.5	99	250	755	2.3	3.02	2.77
14	AO AND PS (B)	210	2	1.5	77	500	404	1.32	1.61	1.59
	TOTAL	5310	146	21	1947	13500	13407	41	53.6	49.5

Table 19.Result of Design

6.4. Selection of outdoor & Indoor Unit Capacity:

6.4.1 Outdoor unit:

SR.NO.	OUTDOOR UNIT	HP
1.	MMY-MAP14A7T8P	14
2.	MMY-MAP14A7T8P	14
3.	MMY-MAP14A7T8P	14
4.	MMY-MAP14A7T8P	14
TOTAL	56	

Table 20. Selection of Outdoor Unit

6.4.2. Indoor unit:

SR NO	NAME OF ROOM	TYPE OF IDU & MODEL NO.	NOS. OF IDU	IDU HP
1.	STAFF AREA-1	4-way cassette MMU-AP0364HP1-E	4	4HP
2.	DCIT-1	4-way cassette MMU-AP0274HP1-E	1	3HP
3.	DCIT-2	4-way cassette MMU-AP0274HP1-E	1	3HP
4.	ITO-1	4-way cassette MMU-AP0274HP1-E	1	3HP
5.	ITO-2	4-way cassette MMU-AP0274HP1-E	1	3HP
6.	ITO-3	4-way cassette MMU-AP0274HP1-E	1	3HP
7.	ITO-4	4-way cassette MMU-AP0274HP1-E	1	3HP
8.	STAFF AREA-2	4-way cassette MMU-AP0364HP1-E	3	4HP
9.	CIT A	4-way cassette MMU-AP0364HP1-E	1	4HP
10.	AO AND PS (A)	4-way cassette MMU-AP0274HP1-E	1	3HP
11.	JCTI-1	4-way cassette MMU-AP0364HP1-E	1	4HP
12.	ADDL JCTI-1	4-way cassette MMU-AP0364HP1-E	1	4HP

13.	CIT (B)	4-way cassette MMU-AP0364HP1-E	1	4HP
14.	AO AND PS (B)	4-way cassette MMU-AP0274HP1-E	1	3HP
TOTAL				68HP

Table 21. Selection of Indoor Unit

$$\text{DIVERSITY} = \frac{\text{INDOOR UNIT CAPACITY}}{\text{OUTDOOR UNIT CAPACITY}} \times 100 = \frac{68}{56} \times 100 = 121\%$$

The outdoor unit & indoor unit models according to the capacity are selected from Toshiba catalogue.

In Toshiba there is a chance to get diversity up to 135% if numbers of occupants are increases in room it will not affects the efficiency of system.

6.5. Pipe Size and Details

Pipe material= copper

For outdoor unit connecting pipe (Model MMY-MAP14A7T8P pipe dimension selected

Gas side = Ø 28.6mm, Liquid side= Ø 15.9mm

Between ODU connection piping kits: - Gas side=Ø41.3mm, Liquid side=Ø22.2mm

IDU connection piping kit of header unit: - Gas side=Ø41.3mm, Liquid side=Ø22.2mm

Between 2 y-joints pipe size differs according to equivalent HP

IDU connecting pipe as per the capacity of IDU

RAFFNATES according to equivalent HP

ODU connecting kit selected as per the equivalent HP

6.6. Insulation:

Standard insulation pipe thickness

Supply pipe insulation=19mm

Return pipe insulation=13mm

CHAPTER 07

7. VALIDATION OF RESULT

JOB : GROUND FLOOR				HEAT LOAD CALCULATIONS			
SPACE : STAFF AREA- 1				DATE	3/10/2020		
				TIME	18:23		
DESIGN DATA				HEAT LOAD SUMMARY			
AREA:	1400			GRAND TOTAL HEAT	10.3		HP
HT.OF THE AREA:	11			DEHUMIDIFIED AIR Cfm	3314		
LIGHTING (WATTS/SQFT)	1.5			TONS AS PER Cfm	8.3		
NO.OF AIR CHANGE REQUIRED	2			TONNAGE REQUIRED	10.3		12.45
Cfm VENTILATION	513			CFM PER SQFT	2.37		
Cfm/PERSON	10			AREA PER TON	135		
NO.OF PEOPLE	30						
Cfm VENTILATION	300						
Cfm VENTILATION IN CAL.	513						
	D.B.	W.B.	%RH	GR/LB			
OUTSIDE	100	83	60	146.0			
INSIDE	75	-	50	64.0			
DIFF.	25	-	-	82.0			
SUN GAIN				BYPASS O.A. LATENT LOAD			
AREA or T.DIFF.		FACTOR	BTU	CFM	G.DIFF	BYPASS	FACTOR
SOLAR GAIN-GLASS				513	82	0.08	0.68
NORTH	0	11	0.56				
SOUTH	0	11	0.56				
EAST	19	11	0.56				
WEST	0	165	0.56				
N-E	0	11	0.56				
N-W	0	118	0.56				
S-E	0	11	0.56				
S-W	0	113	0.56				
SOLAR & TRANSMISSION GAIN				INTERNAL LATENT LOAD			
NORTH	0	20	0.34				
SOUTH	0	36	0.34				
EAST	52	22	0.34				
WEST	363	36	0.34				
N-E	0	17	0.34				
N-W	0	13	0.34				
S-E	0	25	0.34				
S-W	0	21	0.34				
ROOF	1400	51	0.15				
OTHER TRANSMISSION GAIN				ROOM LATENT HEAT			
AGLS	19	25	1.13				
PART	1023	20	0.34				
CEIL	1400	20	0.34				
FLOR	1400	20	0.34				
BYPASS O.A. SENSIBLE LOAD				ROOM TOTAL HEAT			
	CFM	T.DIFF.	FACTOR				
	513	25	0.08				
INTERNAL SENSIBLE LOAD				ROOM LATENT HEAT			
PEOPLE	30	245					
APPL.	5000	3.4					
LIGHTS	2100	3.4	1.25				
FOOD	0	60					
LEAK LOSS +SAFETY FACTOR=5%				ROOM TOTAL HEAT			
				81313			
ROOM SENSIBLE HEAT				OUTSIDE AIR HEAT			
72451							
				HEAT GAIN SAFETY FACTOR @ 3%			
				3612			
				GRAND TOTAL HEAT (TONS)			
				10.3			
				SENSIBLE HEAT FACTOR			
				0.89			
				SELECTED A.D.P.			
				52			
				DEHUMIDIFIED RISE			
				20			
				DEHUMIDIFIED AIR Cfm			
				3314			
				TONS AS PER Cfm			
				8.3			
				CHECK RESULTS.			
				GRAND TOTAL HEAT(BTU/HR/SQFT.)			
				88.58			
				ROOM SENSIBLE HEAT(BTU/HR/SQFT.)			
				51.75			
				SQFT/PERSON			
				46.67			
				TONS PER SQFT			
				0.01			
				CFM PER SQFT			
				2.37			
				TONS/PERSON			
				0.34			
				DEHUMIDIFIED CFM/TON			
				320.73			
				AREA PER TON			
				135.47			

JOB : GROUND FLOOR					HEAT LOAD CALCULATIONS					
SPACE : DCIT - 1					DATE 3/10/2020					
					TIME 18:23					
DESIGN DATA					HEAT LOAD SUMMARY					
AREA:	200				GRAND TOTAL HEAT	1.4				
HT.OF THE AREA:	11				DEHUMIDIFIED AIR Cfm	398				
LIGHTING (WATTS/SQFT)	1.5				TONS AS PER Cfm	1.0				
NO.OF AIR CHANGE REQUIRED	2				TONNAGE REQUIRED	1.4				
Cfm VENTILATION	73				CFM PER SQFT	1.99				
Cfm/PERSON	10				AREA PER TON	144				
NO.OF PEOPLE	7									
Cfm VENTILATION	70									
Cfm VENTILATION IN CAL.	73									
	D.B.	W.B.	%RH	GR/LB						
OUTSIDE	100	83	60	146						
INSIDE	75	-	50	64.0						
DIFF.	25	-	-	82.0						
SUN GAIN					BYPASS O.A. LATENT LOAD					
	AREA	or T.DIFF.	FACTOR	BTU		CFM	G.DIFF.	BYPASS	FACTOR	BTU
SOLAR GAIN-GLASS										
NORTH	0	11	0.56	0		73	82	0.08	0.68	327
SOUTH	0	11	0.56	0	INTERNAL LATENT LOAD					
EAST	0	11	0.56	0	PEOPLE 7 205 1435					
WEST	0	165	0.56	0	SUB TOTAL 1762					
N-E	0	11	0.56	0	SAFETY FACTOR=5% 88					
N-W	0	118	0.56	0	ROOM LATENT HEAT 1850					
S-E	0	11	0.56	0	ROOM TOTAL HEAT 10557					
S-W	0	113	0.56	0	OUTSIDE AIR HEAT					
SOLAR & TRANSMISSION GAIN										
NORTH	0	20	0.34	0		CFM	G.DIFF.	I-B.E.	FACTOR	
SOUTH	0	36	0.34	0	SENS	73	25	0.92	1.08	1822
EAST	0	22	0.34	0	LAT	73	82	0.92	0.68	3762
WEST	0	36	0.34	0	SUB TOTAL 5584					
N-E	0	17	0.34	0	TOTAL 16140					
N-W	0	13	0.34	0	HEAT GAIN SAFETY FACTOR @ 3% 484					
S-E	0	25	0.34	0	GRAND TOTAL HEAT (TONS) 1.4 16625					
S-W	0	21	0.34	0	SENSIBLE HEAT FACTOR 0.82					
ROOF	200	51	0.15	0	SELECTED A.D.P. 52					
OTHER TRANSMISSION GAIN					DEHUMIDIFIED RISE 20					
AGLS	0	25	1.13	0	DEHUMIDIFIED AIR Cfm 398					
PART	176	20	0.34	1197	TONS AS PER Cfm 1.0					
CEIL	200	20	0.34	1	CHECK RESULTS.					
FLOR	200	20	0.34	1	GRAND TOTAL HEAT(BTU/HR/SQFT.) 83.12					
BYPASS O.A. SENSIBLE LOAD					ROOM SENSIBLE HEAT(BTU/HR/SQFT.) 43.53					
	CFM	I.DIFF.	FACTOR		SQFT/PERSON 28.57					
	73	25	0.08	1.08	TONS PER SQFT 0.01					
INTERNAL SENSIBLE LOAD					CFM PER SQFT 1.99					
PEOPLE	7	245		1715	TONS/PERSON 0.20					
APPL	250	3.4		850	DEHUMIDIFIED CFM/TON 287.51					
LIGHTS	300	3.4	1.25	1275	AREA PER TON 144.36					
FOOD	0	60		0						
SUB TOTAL 7915										
LEAK LOSS +SAFETY FACTOR=5% 396										
ROOM SENSIBLE HEAT 8707										

JOB : GROUND FLOOR				HEAT LOAD CALCULATIONS					
SPACE : DCIT - 2				DATE		3/10/2020			
				TIME		18:23			
DESIGN DATA									
AREA:				200					
HT.OF THE AREA:				11					
LIGHTING (WATTS/SQFT)				1.5					
NO.OF AIR CHANGE REQUIRED				2					
Cfm VENTILATION				73					
Cfm/PERSON				10					
NO.OF PEOPLE				7					
Cfm VENTILATION				70					
Cfm VENTILATION IN CAL.				73					
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>	<u>GR/LB</u>					
OUTSIDE	100	83	60	146					
INSIDE	75	-	50	64.0					
DIFF.	25	-	-	82.0					
SUN GAIN				BYPASS O.A. LATENT LOAD					
	<u>AREA</u>	<u>of T.DIFF.</u>	<u>FACTOR</u>	<u>BTU</u>	<u>CFM</u>	<u>G.DIFF</u>	<u>BYPASS</u>	<u>FACTOR</u>	<u>BTU</u>
SOLAR GAIN-GLASS					73	82	0.08	0.68	327
NORTH	0	11	0.56	0					
SOUTH	0	11	0.56	0					
EAST	0	11	0.56	0					
WEST	0	165	0.56	0					
N-E	0	11	0.56	0					
N-W	0	118	0.56	0					
S-E	0	11	0.56	0					
S-W	0	113	0.56	0					
SOLAR & TRANSMISSION GAIN									
NORTH	0	20	0.34	0					
SOUTH	0	36	0.34	0					
EAST	0	22	0.34	0					
WEST	0	36	0.34	0					
N-E	0	17	0.34	0					
N-W	0	13	0.34	0					
S-E	0	25	0.34	0					
S-W	0	21	0.34	0					
ROOF	200	51	0.15	0					
OTHER TRANSMISSION GAIN									
AGLS	0	25	1.13	0					
PART	176	20	0.34	1197					
CEIL	200	20	0.34	1	1360				
FLOR	200	20	0.34	1	1360				
BYPASS O.A. SENSIBLE LOAD									
	<u>CFM</u>	<u>T.DIFF.</u>	<u>FACTOR</u>						
	73	25	0.08	1.08	158				
INTERNAL SENSIBLE LOAD									
PEOPLE	7	245			1715				
APPL.	250	3.4			850				
LIGHTS	300	3.4	1.25		1275				
FOOD	0	60			0				
SUB TOTAL					7915				
LEAKLOSS +SAFETY FACTOR=5%					396				
ROOM SENSIBLE HEAT					8707				
				INTERNAL LATENT LOAD					
				PEOPLE	7	205			1435
				SUB TOTAL					1762
				SAFETY FACTOR=5%					88
				ROOM LATENT HEAT					1850
				ROOM TOTAL HEAT					10557
				OUTSIDE AIR HEAT					
					<u>CFM</u>	<u>G.DIFF</u>	<u>L-B.F.</u>	<u>FACTOR</u>	
				SENS	73	25	0.92	1.08	1822
				LAT	73	82	0.92	0.68	3762
				SUB TOTAL					5584
				TOTAL					16140
				HEAT GAIN SAFETY FACTOR @ 3%					484
				GRAND TOTAL HEAT			(TONS)	1.4	16625
				SENSIBLE HEAT FACTOR				0.82	
				SELECTED A.D.P.				52	
				DEHUMIDIFIED RISE				20	
				DEHUMIDIFIED AIR Cfm				398	
				TONS AS PER Cfm				1.0	
				CHECK RESULTS.					
				GRAND TOTAL HEAT(BTU/HR/SQFT.)				83.12	
				ROOM SENSIBLE HEAT(BTU/HR/SQFT.)				43.53	
				SQFT/PERSON				28.57	
				TONS PER SQFT				0.01	
				CFM PER SQFT				1.99	
				TONS/PERSON				0.20	
				DEHUMIDIFIED CFM/TON				287.51	
				AREA PER TON				144.36	

JOB : GROUND FLOOR				HEAT LOAD CALCULATIONS			
SPACE : ITO - 1				DATE		3/10/2020	
				TIME		18:13	
DESIGN DATA				HEAT LOAD SUMMARY			
AREA:	190			GRAND TOTAL HEAT	1.6		
HT.OF THE AREA:	11			DEHUMIDIFIED AIR Cfm	545		
LIGHTING (WATTS/SQFT)	1.5			TONS AS PER Cfm	1.4		
NO.OF AIR CHANGE REQUIRED	2			TONNAGE REQUIRED	1.6		
Cfm VENTILATION	70			CFM PER SQFT	2.87		
Cfm/PERSON	10			AREA PER TON	118		
NO.OF PEOPLE	6						
Cfm VENTILATION	60						
Cfm VENTILATION IN CAL.	70						
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>	<u>GR/LB</u>			
OUTSIDE	100	83	60	146			
INSIDE	75	-	50	64.0			
DIFF.	25	-	-	82.0			
SUN GAIN				BYPASS O.A. LATENT LOAD			
<u>AREA or T.DIFF. FACTOR</u>			<u>BTU</u>	<u>CFM</u>	<u>G.DIFF</u>	<u>BYPASS FACTOR</u>	<u>BTU</u>
				70	82	0.08	311
SOLAR GAIN-GLASS				INTERNAL LATENT LOAD			
NORTH	44	11	0.56	273	PEOPLE		
SOUTH	0	11	0.56	0	6	205	
EAST	0	11	0.56	0	SUB TOTAL		
WEST	0	165	0.56	0	1541		
N-E	0	11	0.56	0	SAFETY FACTOR=5%		
N-W	0	118	0.56	0	77		
S-E	0	11	0.56	0	ROOM LATENT HEAT		
S-W	0	113	0.56	0	1618		
SOLAR & TRANSMISSION GAIN				ROOM TOTAL HEAT			
NORTH	78	20	0.34	527	13526		
SOUTH	0	36	0.34	0			
EAST	0	22	0.34	0			
WEST	0	36	0.34	0			
N-E	0	17	0.34	0			
N-W	0	13	0.34	0			
S-E	0	25	0.34	0			
S-W	0	21	0.34	0			
ROOF	190	51	0.15	0			
OTHER TRANSMISSION GAIN				OUTSIDE AIR HEAT			
AGLS	44	25	1.13	1252			
PART	369	20	0.34	2507			
CEIL	190	20	0.34	1	1292		
FLOR	190	20	0.34	1	1292		
BYPASS O.A. SENSIBLE LOAD				HEAT GAIN SAFETY FACTOR @ 3%			
	<u>CFM</u>	<u>T.DIFF. FACTOR</u>			565		
	70	25	0.08	1.08	150		
INTERNAL SENSIBLE LOAD				GRAND TOTAL HEAT (TONS)			
PEOPLE	6	245		1470	1.6		
APPL.	250	3.4		850			
LIGHTS	285	3.4	1.25	1211	SENSIBLE HEAT FACTOR		
FOOD	0	60		0	0.88		
SUB TOTAL				10825	SELECTED A.D.P.		
LEAK LOSS +SAFETY FACTOR=5%				541	52		
ROOM SENSIBLE HEAT				11908	DEHUMIDIFIED RISE		
					20		
					DEHUMIDIFIED AIR Cfm		
					545		
					TONS AS PER Cfm		
					1.4		
CHECK RESULTS.							
GRAND TOTAL HEAT(BTU/HR/SQFT.)				102.08			
ROOM SENSIBLE HEAT(BTU/HR/SQFT.)				62.67			
SQFT/PERSON				31.67			
TONS PER SQFT				0.01			
CFM PER SQFT				2.87			
TONS/PERSON				0.27			
DEHUMIDIFIED CFM/TON				337.05			
AREA PER TON				117.56			

JOB : GROUND FLOOR					HEAT LOAD CALCULATIONS				
SPACE : ITO -2					DATE		3/10/2020		
					TIME		18:16		
DESIGN DATA					HEAT LOAD SUMMARY				
AREA:	190				GRAND TOTAL HEAT	1.4		HP	
HT.OF THE AREA:	11				DEHUMIDIFIED AIR Cfm	413			
LIGHTING (WATTS/SQFT)	1.5				TONS AS PER Cfm	1.0			
NO.OF AIR CHANGE REQUIRED	2				TONNAGE REQUIRED	1.4		1.65	
Cfm VENTILATION	70				CFM PER SQFT	2.18			
Cfm/PERSON	10				AREA PER TON	139			
NO.OF PEOPLE	6								
Cfm VENTILATION	60								
Cfm VENTILATION IN CAL.	70								
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>	<u>GR/LB</u>					
OUTSIDE	100	83	60	146					
INSIDE	75	-	50	64.0					
DIFF.	25	-	-	82.0					
SUN GAIN					BYPASS O.A. LATENT LOAD				
<u>AREA or T.DIFF.</u>		<u>FACTOR</u>	<u>BTU</u>		<u>CFM</u>	<u>G.DIFF</u>	<u>BYPASS</u>	<u>FACTOR</u>	<u>BTU</u>
SOLAR GAIN-GLASS					70	82	0.08	0.68	311
NORTH	42	11	0.56	257	INTERNAL LATENT LOAD				
SOUTH	0	11	0.56	0	PEOPLE	6	205	1230	
EAST	0	11	0.56	0	SUB TOTAL				
WEST	0	165	0.56	0	1541				
N-E	0	11	0.56	0	SAFETY FACTOR=5%				
N-W	0	118	0.56	0	77				
S-E	0	11	0.56	0	ROOM LATENT HEAT				
S-W	0	113	0.56	0	1618				
SOLAR & TRANSMISSION GAIN					ROOM TOTAL HEAT				
NORTH	81	20	0.34	554	10656				
SOUTH	0	36	0.34	0	OUTSIDE AIR HEAT				
EAST	0	22	0.34	0	<u>CFM</u>	<u>G.DIFF</u>	<u>L-B.F.</u>	<u>FACTOR</u>	
WEST	0	36	0.34	0	SENS	70	25	0.92	1.08
N-E	0	17	0.34	0	LAT	70	82	0.92	0.68
N-W	0	13	0.34	0	SUB TOTAL				
S-E	0	25	0.34	0	5304				
S-W	0	21	0.34	0	TOTAL				
ROOF	190	51	0.15	0	15960				
OTHER TRANSMISSION GAIN					HEAT GAIN SAFETY FACTOR @ 3%				
AGLS	42	25	1.13	1179	479				
PART	184	20	0.34	1254	GRAND TOTAL HEAT (TONS)				
CEIL	190	20	0.34	1292	1.4				
FLOR	190	20	0.34	0	16439				
BYPASS O.A. SENSIBLE LOAD					SENSIBLE HEAT FACTOR				
	<u>CFM</u>	<u>T.DIFF.</u>	<u>FACTOR</u>		0.85				
	70	25	0.08	1.08	150				
INTERNAL SENSIBLE LOAD					SELECTED A.D.P.				
PEOPLE	6	245	1470		52				
APPL	250	3.4	850		20				
LIGHTS	285	3.4	1.25	1211	DEHUMIDIFIED AIR Cfm				
FOOD	0	60	0		413				
SUB TOTAL					TONS AS PER Cfm				
8217					1.0				
LEAK LOSS +SAFETY FACTOR=5%					CHECK RESULTS.				
411					GRAND TOTAL HEAT(BTU/HR/SQFT.)				
ROOM SENSIBLE HEAT					86.52				
9038					ROOM SENSIBLE HEAT(BTU/HR/SQFT.)				
					47.57				
					SQFT/PERSON				
					31.67				
					TONS PER SQFT				
					0.01				
					CFM PER SQFT				
					2.18				
					TONS/PERSON				
					0.23				
					DEHUMIDIFIED CFM/TON				
					301.82				
					AREA PER TON				
					138.69				

JOB : GROUND FLOOR		HEAT LOAD CALCULATIONS	
SPACE : ITO - 3		DATE	3/10/2020
		TIME	18:32
DESIGN DATA			
AREA:	190		
HT.OF THE AREA:	11		
LIGHTING (WATTS/SQFT)	1.5		
NO.OF AIR CHANGE REQUIRED	2		
Cfm VENTILATION	70		
Cfm/PERSON	10		
NO.OF PEOPLE	6		
Cfm VENTILATION	60		
Cfm VENTILATION IN CAL.	70		
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>
OUTSIDE	100	83	60
INSIDE	75	-	50
DIFF.	25	-	82.0
		HEAT LOAD SUMMARY	
		TR	HP
GRAND TOTAL HEAT		1.5	
DEHUMIDIFIED AIR Cfm		507	
TONS AS PER Cfm		1.3	
TONNAGE REQUIRED		1.5	1.86
CFM PER SQFT		2.67	
AREA PER TON		123	
SUN GAIN			
<u>AREA</u>	<u>or T.DIFF.</u>	<u>FACTOR</u>	<u>BTU</u>
SOLAR GAIN-GLASS			
NORTH	39	11	0.56
SOUTH	0	11	0.56
EAST	57	11	0.56
WEST	0	165	0.56
N-E	0	11	0.56
N-W	0	118	0.56
S-E	0	11	0.56
S-W	0	113	0.56
SOLAR & TRANSMISSION GAIN			
NORTH	81	20	0.34
SOUTH	0	36	0.34
EAST	0	22	0.34
WEST	0	36	0.34
N-E	0	17	0.34
N-W	0	13	0.34
S-E	0	25	0.34
S-W	0	21	0.34
ROOF	190	51	0.15
OTHER TRANSMISSION GAIN			
AGLS	96	25	1.13
PART	184	20	0.34
CEIL	190	20	0.34
FLOR	190	20	0.34
BYPASS O.A. SENSIBLE LOAD			
<u>CFM</u>	<u>T.DIFF.</u>	<u>FACTOR</u>	
70	25	0.08	1.08
INTERNAL SENSIBLE LOAD			
PEOPLE	6	245	1470
APPL.	250	3.4	850
LIGHTS	285	3.4	1.25
FOOD	0	60	
SUB TOTAL			10073
LEAK LOSS +SAFETY FACTOR=5%			
			504
ROOM SENSIBLE HEAT			11080
BYPASS O.A. LATENT LOAD			
<u>CFM</u>	<u>G.DIFF.</u>	<u>BYPASS</u>	<u>FACTOR</u>
70	82	0.08	0.68
INTERNAL LATENT LOAD			
PEOPLE	6	205	1230
SUB TOTAL			
			1541
SAFETY FACTOR=5%			
			77
ROOM LATENT HEAT			
			1618
ROOM TOTAL HEAT			
			12698
OUTSIDE AIR HEAT			
<u>SENS</u>	<u>CFM</u>	<u>G.DIFF.</u>	<u>I-B.E. FACTOR</u>
	70	25	0.92
<u>LAT</u>	70	82	0.92
SUB TOTAL			
			5304
TOTAL			
			18002
HEAT GAIN SAFETY FACTOR @ 3%			
			540
GRAND TOTAL HEAT (TONS)			
			1.5
SENSIBLE HEAT FACTOR			
			0.87
SELECTED A.D.P.			
			52
DEHUMIDIFIED RISE			
			20
DEHUMIDIFIED AIR Cfm			
			507
TONS AS PER Cfm			
			1.3
CHECK RESULTS.			
GRAND TOTAL HEAT(BTU/HR/SQFT.)			97.59
ROOM SENSIBLE HEAT(BTU/HR/SQFT.)			58.32
SQFT/PERSON			31.67
TONS PER SQFT			0.01
CFM PER SQFT			2.67
TONS/PERSON			0.26
DEHUMIDIFIED CFM/TON			328.04
AREA PER TON			122.96

JOB : GROUND FLOOR					HEAT LOAD CALCULATIONS																								
SPACE : ITO - 4					DATE		3/10/2020																						
					TIME		18:32																						
DESIGN DATA					HEAT LOAD SUMMARY																								
AREA: 190					GRAND TOTAL HEAT 1.6 HP																								
HT.OF THE AREA: 11					DEHUMIDIFIED AIR Cfm 530																								
LIGHTING (WATTS/SQFT) 1.5					TONS AS PER Cfm 1.3																								
NO.OF AIR CHANGE REQUIRED 2					TONNAGE REQUIRED 1.6 1.91																								
Cfm VENTILATION 70					CFM PER SQFT 2.79																								
Cfm/PERSON 10					AREA PER TON 120																								
NO.OF PEOPLE 6																													
Cfm VENTILATION 60																													
Cfm VENTILATION IN CAL. 70																													
<table border="1"> <thead> <tr> <th></th> <th>D.B.</th> <th>W.B.</th> <th>%RH</th> <th>GR/LB</th> </tr> </thead> <tbody> <tr> <td>OUTSIDE</td> <td>100</td> <td>83</td> <td>60</td> <td>146</td> </tr> <tr> <td>INSIDE</td> <td>75</td> <td>-</td> <td>50</td> <td>64.0</td> </tr> <tr> <td>DIFF.</td> <td>25</td> <td>-</td> <td>-</td> <td>82.0</td> </tr> </tbody> </table>						D.B.	W.B.	%RH	GR/LB	OUTSIDE	100	83	60	146	INSIDE	75	-	50	64.0	DIFF.	25	-	-	82.0					
	D.B.	W.B.	%RH	GR/LB																									
OUTSIDE	100	83	60	146																									
INSIDE	75	-	50	64.0																									
DIFF.	25	-	-	82.0																									
SUN GAIN					BYPASS O.A. LATENT LOAD																								
AREA or T.DIFF. FACTOR BTU					CFM G.DIFF BYPASS FACTOR BTU																								
SOLAR GAIN-GLASS					70 82 0.08 0.68 311																								
NORTH	39	11	0.56	238	INTERNAL LATENT LOAD																								
SOUTH	0	11	0.56	0	PEOPLE 6 205 1230																								
EAST	32	11	0.56	200	SUB TOTAL 1541																								
WEST	0	165	0.56	0	SAFETY FACTOR=5% 77																								
N-E	0	11	0.56	0	ROOM LATENT HEAT 1618																								
N-W	0	118	0.56	0	ROOM TOTAL HEAT 13210																								
S-E	0	11	0.56	0	OUTSIDE AIR HEAT																								
S-W	0	113	0.56	0	CFM G.DIFF I-B.F. FACTOR																								
SOLAR & TRANSMISSION GAIN					SENS 70 25 0.92 1.08 1731																								
NORTH	92	20	0.34	626	LAT 70 82 0.92 0.68 3574																								
SOUTH	0	36	0.34	0	SUB TOTAL 5304																								
EAST	160	22	0.34	1198	TOTAL 18514																								
WEST	0	36	0.34	0	HEAT GAIN SAFETY FACTOR @ 3% 555																								
N-E	0	17	0.34	0	GRAND TOTAL HEAT (TONS) 1.6 19070																								
N-W	0	13	0.34	0	SENSIBLE HEAT FACTOR 0.88																								
S-E	0	25	0.34	0	SELECTED A.D.P. 52																								
S-W	0	21	0.34	0	DEHUMIDIFIED RISE 20																								
ROOF	190	51	0.15	0	DEHUMIDIFIED AIR Cfm 530																								
OTHER TRANSMISSION GAIN					TONS AS PER Cfm 1.3																								
AGLS	71	25	1.13	2010	CHECK RESULTS.																								
PART	0	20	0.34	0	GRAND TOTAL HEAT(BTU/HR/SQFT.) 100.37																								
CEIL	190	20	0.34	1 1292	ROOM SENSIBLE HEAT(BTU/HR/SQFT.) 61.01																								
FLOOR	190	20	0.34	1 1292	SQFT/PERSON 31.67																								
BYPASS O.A. SENSIBLE LOAD					TONS PER SQFT 0.01																								
CFM T.DIFF. FACTOR					CFM PER SQFT 2.79																								
70 25 0.08 1.08 150					TONS/PERSON 0.26																								
INTERNAL SENSIBLE LOAD					DEHUMIDIFIED CFM/TON 333.71																								
PEOPLE	6	245		1470	AREA PER TON 119.56																								
APPL.	250	3.4		850																									
LIGHTS	285	3.4	1.25	1211																									
FOOD	0	60		0																									
SUB TOTAL 10538																													
LEAK LOSS +SAFETY FACTOR=5% 527																													
ROOM SENSIBLE HEAT 11592																													

JOB : GROUND FLOOR				HEAT LOAD CALCULATIONS						
SPACE : STAFF AREA - 2				DATE		3/10/2020				
				TIME		18:32				
DESIGN DATA										
AREA:				1200						
HT.OF THE AREA:				11						
LIGHTING (WATTS/SQFT)				1.5						
NO.OF AIR CHANGE REQUIRED				2						
Cfm VENTILATION				440						
Cfm/PERSON				10						
NO.OF PEOPLE				30						
Cfm VENTILATION				300						
Cfm VENTILATION IN CAL.				440						
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>	<u>GR/LB</u>						
OUTSIDE	100	83	60	146.0						
INSIDE	75	-	50	64.0						
DIFF.	25	-	-	82.0						
				HEAT LOAD SUMMARY		TR				
				GRAND TOTAL HEAT		9.6				
				DEHUMIDIFIED AIR Cfm		3180				
				TONS AS PER Cfm		8.0				
				TONNAGE REQUIRED		9.6				
						11.53				
				CFM PER SQFT		2.65				
				AREA PER TON		125				
SUN GAIN				BYPASS O.A. LATENT LOAD						
		<u>AREA or T.DIFF.</u>	<u>FACTOR</u>			<u>CFM</u>	<u>G.DIFF</u>	<u>BYPASS</u>	<u>FACTOR</u>	<u>BTU</u>
SOLAR GAIN-GLASS						440	82	0.08	0.68	1963
NORTH	141	11	0.56							871
SOUTH	0	11	0.56							0
EAST	0	11	0.56							0
WEST	0	165	0.56							0
N-E	0	11	0.56							0
N-W	0	118	0.56							0
S-E	0	11	0.56							0
S-W	0	113	0.56							0
SOLAR & TRANSMISSION GAIN										758
NORTH	112	20	0.34							0
SOUTH	0	36	0.34							0
EAST	0	22	0.34							0
WEST	0	36	0.34							0
N-E	0	17	0.34							0
N-W	0	13	0.34							0
S-E	0	25	0.34							0
S-W	0	21	0.34							0
ROOF	1200	51	0.15	0					0	
OTHER TRANSMISSION GAIN										3996
AGLS	141	25	1.13							8303
PART	1221	20	0.34							8160
CEIL	1200	20	0.34	1					8160	
FLOR	1200	20	0.34	1					8160	
BYPASS O.A. SENSIBLE LOAD										950
		<u>CFM</u>	<u>T.DIFF.</u>	<u>FACTOR</u>						
		440	25	0.08	1.08					
INTERNAL SENSIBLE LOAD										7350
PEOPLE	30	245								
APPL	5000	3.4								
LIGHTS	1800	3.4	1.25							7650
FOOD	0	60								
SUB TOT,	55									63199
LEAK LOSS +SAFETY FACTOR=5%										3160
ROOM SENSIBLE HEAT										69519
										6150
										8113
										406
										8518
										78038
										10930
										22572
										33501
										111539
										3346
										114885
										0.89
										52
										20
										3180
										8.0
										40.00
										2.65
										0.32
										332.19
										125.34

JOB : GROUND FLOOR						
SPACE : CIT A				HEAT LOAD CALCULATIONS		
				DATE	3/10/2020	
				TIME	18:32	
DESIGN DATA						
AREA:					270	
HT.OF THE AREA:					11	
LIGHTING (WATTS/SQFT)					1.5	
NO.OF AIR CHANGE REQUIRED					2	
Cfm VENTILATION					99	
Cfm/PERSON					10	
NO.OF PEOPLE					10	
Cfm VENTILATION					100	
Cfm VENTILATION IN CAL.					100	
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>	<u>GR/LB</u>		
OUTSIDE	100	83	60	146		
INSIDE	75	-	50	64.0		
DIFF.	25	-	-	82.0		
HEAT LOAD SUMMARY						
				TR	HP	
GRAND TOTAL HEAT					2.3	
DEHUMIDIFIED AIR Cfm					745	
				1.9	2.74	
TONS AS PER Cfm					2.3	
TONNAGE REQUIRED					2.76	
CFM PER SQFT					119	
AREA PER TON						
SUN GAIN						
<u>AREA or T.DIFF. FACTOR</u>				<u>BTU</u>		
SOLAR GAIN-GLASS						
NORTH	26	11	0.56	158		
SOUTH	0	11	0.56	0		
EAST	51	11	0.56	317		
WEST	0	165	0.56	0		
N-E	0	11	0.56	0		
N-W	0	118	0.56	0		
S-E	0	11	0.56	0		
S-W	0	113	0.56	0		
SOLAR & TRANSMISSION GAIN						
NORTH	130	20	0.34	883		
SOUTH	0	36	0.34	0		
EAST	181	22	0.34	1357		
WEST	0	36	0.34	0		
N-E	0	17	0.34	0		
N-W	0	13	0.34	0		
S-E	0	25	0.34	0		
S-W	0	21	0.34	0		
ROOF	270	51	0.15	0	0	
OTHER TRANSMISSION GAIN						
AGLS	77	25	1.13	2180		
PART	147	20	0.34	998		
CEIL	270	20	0.34	1	1836	
FLOR	270	20	0.34	1	1836	
BYPASS O.A. SENSIBLE LOAD						
<u>CFM T.DIFF. FACTOR</u>				<u>BTU</u>		
				100	25	0.08
				1.08	216	
INTERNAL SENSIBLE LOAD						
PEOPLE	10	245			2450	
APPL	250	3.4			850	
LIGHTS	405	3.4	1.25	1721		
FOOD	0	60			0	
SUB TOTAL					14802	
				740		
LEAK LOSS +SAFETY FACTOR=5%					740	
ROOM SENSIBLE HEAT					16282	
BYPASS O.A. LATENT LOAD						
<u>CFM G.DIFF. BYPASS FACTOR</u>				<u>BTU</u>		
				100	82	0.08
				0.68	446	
INTERNAL LATENT LOAD						
PEOPLE	10	205			2050	
SUB TOTAL					2496	
				125		
SAFETY FACTOR=5%					125	
ROOM LATENT HEAT					2621	
ROOM TOTAL HEAT					18903	
OUTSIDE AIR HEAT						
<u>CFM G.DIFF. 1-B.F. FACTOR</u>						
				100	25	0.92
				1.08	2484	
				100	82	0.92
				0.68	5130	
SUB TOTAL					7614	
TOTAL					26517	
				796		
HEAT GAIN SAFETY FACTOR @ 3%					796	
GRAND TOTAL HEAT	(TONS)				2.3	27313
SENSIBLE HEAT FACTOR						
SELECTED A.D.P.					0.86	
DEHUMIDIFIED RISE					52	
				20		
DEHUMIDIFIED AIR Cfm					745	
TONS AS PER Cfm					1.9	
CHECK RESULTS.						
GRAND TOTAL HEAT(BTU/HR/SQFT.)					101.16	
ROOM SENSIBLE HEAT(BTU/HR/SQFT.)					60.30	
SQFT/PERSON					27.00	
TONS PER SQFT					0.01	
CFM PER SQFT					2.76	
TONS/PERSON					0.23	
DEHUMIDIFIED CFM/TON					327.26	
AREA PER TON					118.63	

JOB : GROUND FLOOR					HEAT LOAD CALCULATIONS					
SPACE : AO AND PSA					DATE 3/10/2020					
					TIME 18:32					
DESIGN DATA										
AREA:					240					
HT.OF THE AREA:					11					
LIGHTING (WATTS/SQFT)					1.5					
NO.OF AIR CHANGE REQUIRED					2					
Cfm VENTILATION					88					
Cfm/PERSON					10					
NO.OF PEOPLE					6					
Cfm VENTILATION					60					
Cfm VENTILATION IN CAL.					88					
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>	<u>GR/LB</u>						
OUTSIDE	100	83	60	146						
INSIDE	75	-	50	64.0						
DIFF.	25	-	-	82.0						
					HEAT LOAD SUMMARY TR HP					
					GRAND TOTAL HEAT 1.9					
					DEHUMIDIFIED AIR Cfm 602					
					TONS AS PER Cfm 1.5					
					TONNAGE REQUIRED 1.9 2.23					
					CFM PER SQFT 2.51					
					AREA PER TON 130					
SUN GAIN					BYPASS O.A. LATENT LOAD					
<u>AREA or T.DIFF. FACTOR BTU</u>					<u>CFM G.DIFF. BYPASS FACTOR BTU</u>					
SOLAR GAIN-GLASS					88 82 0.08 0.68 393					
NORTH	0	11	0.56	0	INTERNAL LATENT LOAD					
SOUTH	0	11	0.56	0	PEOPLE 6 205 1230					
EAST	51	11	0.56	317	SUB TOTAL 1623					
WEST	0	165	0.56	0	SAFETY FACTOR=5% 81					
N-E	0	11	0.56	0	ROOM LATENT HEAT 1704					
N-W	0	118	0.56	0	ROOM TOTAL HEAT 14857					
S-E	0	11	0.56	0	OUTSIDE AIR HEAT					
S-W	0	113	0.56	0	<u>CFM G.DIFF. I-B.F. FACTOR</u>					
SOLAR & TRANSMISSION GAIN					SENS 88 25 0.92 1.08 2186					
NORTH	0	20	0.34	0	LAT 88 82 0.92 0.68 4514					
SOUTH	0	36	0.34	0	SUB TOTAL 6700					
EAST	153	22	0.34	1146	TOTAL 21557					
WEST	0	36	0.34	0	HEAT GAIN SAFETY FACTOR @ 3% 647					
N-E	0	17	0.34	0	GRAND TOTAL HEAT (TONS) 1.9 22204					
N-W	0	13	0.34	0	SENSIBLE HEAT FACTOR 0.89					
S-E	0	25	0.34	0	SELECTED A.D.P. 52					
S-W	0	21	0.34	0	DEHUMIDIFIED RISE 20					
ROOF	240	51	0.15	0	DEHUMIDIFIED AIR Cfm 602					
OTHER TRANSMISSION GAIN					TONS AS PER Cfm 1.5					
AGLS	51	25	1.13	1453	CHECK RESULTS.					
PART	131	20	0.34	888	GRAND TOTAL HEAT(BTU/HR/SQFT.) 92.52					
CEIL	240	20	0.34	1 1632	ROOM SENSIBLE HEAT(BTU/HR/SQFT.) 54.81					
FLOR	240	20	0.34	1 1632	SQFT/PERSON 40.00					
BYPASS O.A. SENSIBLE LOAD					TONS PER SQFT 0.01					
<u>CFM T.DIFF. FACTOR</u>					CFM PER SQFT 2.51					
88 25 0.08 1.08 190					TONS/PERSON 0.31					
INTERNAL SENSIBLE LOAD					DEHUMIDIFIED CFM/TON 325.20					
PEOPLE	6	245		1470	AREA PER TON 129.71					
APPL.	500	3.4		1700						
LIGHTS	360	3.4	1.25	1530						
FOOD	0	60		0						
SUB TOTAL					11958					
LEAKLOSS +SAFETY FACTOR=5%					598					
ROOM SENSIBLE HEAT					13153					

JOB : GROUND FLOOR				HEAT LOAD CALCULATIONS					
SPACE : JCTI - 1				DATE		3/10/2020			
				TIME		18:32			
DESIGN DATA				HEAT LOAD SUMMARY					
AREA:				TR	HP				
HT.OF THE AREA:	290			GRAND TOTAL HEAT	2.5				
LIGHTING (WATTS/SQFT)	1.5			DEHUMIDIFIED AIR Cfm	832				
NO.OF AIR CHANGE REQUIRED	2			TONS AS PER Cfm	2.1				
Cfm VENTILATION	106			TONNAGE REQUIRED	2.99				
Cfm/PERSON	10			CFM PER SQFT	2.87				
NO.OF PEOPLE	10			AREA PER TON	117				
Cfm VENTILATION	100								
Cfm VENTILATION IN CAL.	106								
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>	<u>GR/LB</u>					
OUTSIDE	100	83	60	146					
INSIDE	75	-	50	64.0					
DIFF.	25	-	-	82.0					
SUN GAIN				BYPASS O.A. LATENT LOAD					
	<u>AREA</u>	<u>or T.DIFF.</u>	<u>FACTOR</u>	<u>BTU</u>	<u>CFM</u>	<u>G.DIFF</u>	<u>BYPASS</u>	<u>FACTOR</u>	<u>BTU</u>
SOLAR GAIN-GLASS					106	82	0.08	0.68	474
NORTH	0	11	0.56	0	INTERNAL LATENT LOAD				
SOUTH	30	11	0.56	187	PEOPLE	10	205	2050	
EAST	51	11	0.56	317	SUB TOTAL				
WEST	0	165	0.56	0	2524				
N-E	0	11	0.56	0	SAFETY FACTOR=5%				
N-W	0	118	0.56	0	126				
S-E	0	11	0.56	0	ROOM LATENT HEAT				
S-W	0	113	0.56	0	2651				
SOLAR & TRANSMISSION GAIN					ROOM TOTAL HEAT				
NORTH	0	20	0.34	0	20832				
SOUTH	161	36	0.34	1975	OUTSIDE AIR HEAT				
EAST	144	22	0.34	1074		<u>CFM</u>	<u>G.DIFF</u>	<u>I-B.F.</u>	<u>FACTOR</u>
WEST	0	36	0.34	0	SENS	106	25	0.92	1.08
N-E	0	17	0.34	0	LAT	106	82	0.92	0.68
N-W	0	13	0.34	0	SUB TOTAL				
S-E	0	25	0.34	0	8096				
S-W	0	21	0.34	0	TOTAL				
ROOF	290	51	0.15	0	28928				
OTHER TRANSMISSION GAIN					HEAT GAIN SAFETY FACTOR @ 3%				
AGLS	82	25	1.13	2311	868				
PART	197	20	0.34	1342	GRAND TOTAL HEAT (TONS)				
CEIL	290	20	0.34	1972	2.5				
FLOR	290	20	0.34	1972	29796				
BYPASS O.A. SENSIBLE LOAD					SENSIBLE HEAT FACTOR				
	<u>CFM</u>	<u>T.DIFF.</u>	<u>FACTOR</u>		0.87				
	106	25	0.08	1.08	230	SELECTED A.D.P.			
INTERNAL SENSIBLE LOAD					20				
PEOPLE	10	245		2450	DEHUMIDIFIED AIR Cfm				
APPL.	250	3.4		850	832				
LIGHTS	435	3.4	1.25	1849	TONS AS PER Cfm				
FOOD	0	60		0	2.1				
SUB TOTAL				16528	CHECK RESULTS.				
LEAK LOSS +SAFETY FACTOR=5%				826	GRAND TOTAL HEAT(BTU/HR/SQFT.)				
ROOM SENSIBLE HEAT				18181	102.74				
					ROOM SENSIBLE HEAT(BTU/HR/SQFT.)				
					62.69				
					SQFT/PERSON				
					29.00				
					TONS PER SQFT				
					0.01				
					CFM PER SQFT				
					2.87				
					TONS/PERSON				
					0.25				
					DEHUMIDIFIED CFM/TON				
					334.98				
					AREA PER TON				
					116.80				

JOB : GROUND FLOOR				HEAT LOAD CALCULATIONS	
SPACE : ADDL JCTI -1				DATE	3/10/2020
				TIME	18:32
DESIGN DATA					
AREA:	270				
HT.OF THE AREA:	11				
LIGHTING (WATTS/SQFT)	1.5				
NO.OF AIR CHANGE REQUIRED	2				
Cfm VENTILATION	99				
Cfm/PERSON	10				
NO.OF PEOPLE	10				
Cfm VENTILATION	100				
Cfm VENTILATION IN CAL.	100				
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>		
OUTSIDE	100	83	60	146	
INSIDE	75	-	50	64.0	
DIFF.	25	-	-	82.0	
HEAT LOAD SUMMARY					
GRAND TOTAL HEAT	2.1				TR
DEHUMIDIFIED AIR Cfm	660				HP
TONS AS PER Cfm	1.6				
TONNAGE REQUIRED	2.1				2.55
CFM PER SQFT	2.44				
AREA PER TON	128				
SUN GAIN					
	<u>AREA</u>	<u>or T.DIFF.</u>	<u>FACTOR</u>		
				BTU	
SOLAR GAIN-GLASS					
NORTH	0	11	0.56	0	
SOUTH	38	11	0.56	237	
EAST	0	11	0.56	0	
WEST	0	165	0.56	0	
N-E	0	11	0.56	0	
N-W	0	118	0.56	0	
S-E	0	11	0.56	0	
S-W	0	113	0.56	0	
SOLAR & TRANSMISSION GAIN					
NORTH	0	20	0.34	0	
SOUTH	126	36	0.34	1536	
EAST	0	22	0.34	0	
WEST	0	36	0.34	0	
N-E	0	17	0.34	0	
N-W	0	13	0.34	0	
S-E	0	25	0.34	0	
S-W	0	21	0.34	0	
ROOF	270	51	0.15	0	0
OTHER TRANSMISSION GAIN					
AGLS	38	25	1.13	1085	
PART	197	20	0.34	1342	
CEIL	270	20	0.34	1	1836
FLOOR	270	20	0.34	1	1836
BYPASS O.A. SENSIBLE LOAD					
	<u>CFM</u>	<u>T.DIFF.</u>	<u>FACTOR</u>		
	100	25	0.08	1.08	216
INTERNAL SENSIBLE LOAD					
PEOPLE	10	245			2450
APPL.	250	3.4			850
LIGHTS	405	3.4	1.25	1721	
FOOD	0	60			0
SUB TOTAL					13109
LEAK LOSS +SAFETY FACTOR=5%					655
ROOM SENSIBLE HEAT					14419
BYPASS O.A. LATENT LOAD					
	<u>CFM</u>	<u>G.DIFF.</u>	<u>BYPASS</u>	<u>FACTOR</u>	
	100	82	0.08	0.68	446
INTERNAL LATENT LOAD					
PEOPLE	10	205			2050
SUB TOTAL					2496
SAFETY FACTOR=5%					125
ROOM LATENT HEAT					2621
ROOM TOTAL HEAT					17040
OUTSIDE AIR HEAT					
	<u>CFM</u>	<u>G.DIFF.</u>	<u>I-B.E.</u>	<u>FACTOR</u>	
SENS	100	25	0.92	1.08	2484
LAT	100	82	0.92	0.68	5130
SUB TOTAL					7614
TOTAL					24654
HEAT GAIN SAFETY FACTOR @ 3%					740
GRAND TOTAL HEAT	(TONS) 2.1				25394
SENSIBLE HEAT FACTOR					
SELECTED A.D.P.					0.85
DEHUMIDIFIED RISE					52
DEHUMIDIFIED AIR Cfm					20
TONS AS PER Cfm					660
					1.6
CHECK RESULTS.					
GRAND TOTAL HEAT(BTU/HR/SQFT.)					94.05
ROOM SENSIBLE HEAT(BTU/HR/SQFT.)					53.41
SQFT/PERSON					27.00
TONS PER SQFT					0.01
CFM PER SQFT					2.44
TONS/PERSON					0.21
DEHUMIDIFIED CFM/TON					311.72
AREA PER TON					127.59

JOB : GROUND FLOOR					HEAT LOAD CALCULATIONS					
SPACE : CIT (B)					DATE 3/10/2020					
					TIME 18:32					
DESIGN DATA										
AREA:					270					
HT.OF THE AREA:					11					
LIGHTING (WATTS/SQFT)					1.5					
NO.OF AIR CHANGE REQUIRED					2					
Cfm VENTILATION					99					
Cfm/PERSON					10					
NO.OF PEOPLE					10					
Cfm VENTILATION					100					
Cfm VENTILATION IN CAL.					100					
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>	<u>GR/LB</u>						
OUTSIDE	100	83	60	146						
INSIDE	75	-	50	64.0						
DIFF.	25	-	-	82.0						
HEAT LOAD SUMMARY					TR	HP				
GRAND TOTAL HEAT					2.3					
DEHUMIDIFIED AIR Cfm					746					
TONS AS PER Cfm					1.9					
TONNAGE REQUIRED					2.3	2.75				
CFM PER SQFT					2.76					
AREA PER TON					118					
SUN GAIN					BYPASS O.A. LATENT LOAD					
<u>AREA or T.DIFF. FACTOR</u>					<u>CFM</u>	<u>G.DIFF</u>	<u>BYPASS FACTOR</u>	<u>BTU</u>		
					100	82	0.08	0.68	446	
SOLAR GAIN-GLASS					INTERNAL LATENT LOAD					
NORTH	0	11	0.56	0	PEOPLE	10	205	2050		
SOUTH	34	11	0.56	210	SUB TOTAL					
EAST	0	11	0.56	0	2496					
WEST	0	165	0.56	0	SAFETY FACTOR=5%					
N-E	0	11	0.56	0	125					
N-W	0	118	0.56	0	ROOM LATENT HEAT					
S-E	0	11	0.56	0	2621					
S-W	0	113	0.56	0	ROOM TOTAL HEAT					
					18937					
SOLAR & TRANSMISSION GAIN					OUTSIDE AIR HEAT					
NORTH	0	20	0.34	0	<u>CFM</u>					
SOUTH	153	36	0.34	1876	<u>G.DIFF</u>	<u>1-B.E. FACTOR</u>				
EAST	0	22	0.34	0	SENS	100	25	0.92	1.08	2484
WEST	79	36	0.34	963	LAT	100	82	0.92	0.68	5130
N-E	0	17	0.34	0	SUB TOTAL					
N-W	0	13	0.34	0	7614					
S-E	0	25	0.34	0	TOTAL					
S-W	0	21	0.34	0	26550					
ROOF	270	51	0.15	0	HEAT GAIN SAFETY FACTOR @ 3%					
					797					
OTHER TRANSMISSION GAIN					GRAND TOTAL HEAT (TONS)					
AGLS	34	25	1.13	965	2.3					
PART	281	20	0.34	1909	27347					
CEIL	270	20	0.34	1836	SENSIBLE HEAT FACTOR					
FLOR	270	20	0.34	1836	0.86					
BYPASS O.A. SENSIBLE LOAD					SELECTED A.D.P.					
<u>CFM</u>					52					
<u>T.DIFF. FACTOR</u>					DEHUMIDIFIED RISE					
100					20					
25					DEHUMIDIFIED AIR Cfm					
0.08					746					
1.08					TONS AS PER Cfm					
216					1.9					
INTERNAL SENSIBLE LOAD					CHECK RESULTS.					
PEOPLE	10	245	2450		GRAND TOTAL HEAT(BTU/HR/SQFT.)					
APPL	250	3.4	850		101.29					
LIGHTS	405	3.4	1.25	1721	ROOM SENSIBLE HEAT(BTU/HR/SQFT.)					
FOOD	0	60	0		60.43					
SUB TOTAL					SQFT/PERSON					
14832					27.00					
LEAK LOSS +SAFETY FACTOR=5%					TONS PER SQFT					
742					0.01					
ROOM SENSIBLE HEAT					CFM PER SQFT					
16316					2.76					
					TONS/PERSON					
					0.23					
					DEHUMIDIFIED CFM/TON					
					327.52					
					AREA PER TON					
					118.48					

JOB : GROUND FLOOR					HEAT LOAD CALCULATIONS					
SPACE : AO AND PS (B)					DATE	3/10/2020				
					TIME	18:32				
DESIGN DATA					HEAT LOAD SUMMARY					
AREA:	210				GRAND TOTAL HEAT	1.3		TR		HP
HT.OF THE AREA:	11				DEHUMIDIFIED AIR Cfm	399				
LIGHTING (WATTS/SQFT)	1.5				TONS AS PER Cfm	1.0				
NO.OF AIR CHANGE REQUIRED	2				TONNAGE REQUIRED	1.3		1.59		
Cfm VENTILATION	77				CFM PER SQFT	1.90				
Cfm/PERSON	10				AREA PER TON	159				
NO.OF PEOPLE	2									
Cfm VENTILATION	20									
Cfm VENTILATION IN CAL.	77									
	<u>D.B.</u>	<u>W.B.</u>	<u>%RH</u>	<u>GR/LB</u>						
OUTSIDE	100	83	60	146						
INSIDE	75	-	50	64.0						
DIFF.	25	-	-	82.0						
SUN GAIN					BYPASS O.A. LATENT LOAD					
	<u>AREA</u> or <u>T.DIFF.</u>	<u>FACTOR</u>			<u>CFM</u>	<u>G.DIFF</u>	<u>BYPASS</u>	<u>FACTOR</u>	<u>BTU</u>	
SOLAR GAIN-GLASS					77	82	0.08	0.68	343	
NORTH	0	11	0.56	0	INTERNAL LATENT LOAD					
SOUTH	0	11	0.56	0	PEOPLE					
EAST	0	11	0.56	0	2	205		410		
WEST	0	165	0.56	0	SUB TOTAL					
N-E	0	11	0.56	0	753					
N-W	0	118	0.56	0	SAFETY FACTOR=5%					
S-E	0	11	0.56	0	38					
S-W	0	113	0.56	0	ROOM LATENT HEAT					
					791					
					ROOM TOTAL HEAT					
					9522					
SOLAR & TRANSMISSION GAIN					OUTSIDE AIR HEAT					
NORTH	0	20	0.34	0	<u>CFM</u>	<u>G.DIFF</u>	<u>I-B.F.</u>	<u>FACTOR</u>		
SOUTH	0	36	0.34	0	77	25	0.92	1.08	1913	
EAST	0	22	0.34	0	77	82	0.92	0.68	3950	
WEST	0	36	0.34	0	SUB TOTAL					
N-E	0	17	0.34	0	5863					
N-W	0	13	0.34	0	TOTAL					
S-E	0	25	0.34	0	15385					
S-W	0	21	0.34	0	HEAT GAIN SAFETY FACTOR @ 3%					
ROOF	210	51	0.15	0	462					
					GRAND TOTAL HEAT (TONS)					
					1.3 15846					
OTHER TRANSMISSION GAIN					SENSIBLE HEAT FACTOR					
AGLS	0	25	1.13	0	0.92					
PART	204	20	0.34	1386	SELECTED A.D.P.					
CEIL	210	20	0.34	1	52					
FLOR	210	20	0.34	1	20					
					DEHUMIDIFIED RISE					
					399					
					TONS AS PER Cfm					
					1.0					
BYPASS O.A. SENSIBLE LOAD					CHECK RESULTS.					
	<u>CFM</u>	<u>T.DIFF.</u>	<u>FACTOR</u>		GRAND TOTAL HEAT(BTU/HR/SQFT.)					
	77	25	0.08	1.08	75.46					
					ROOM SENSIBLE HEAT(BTU/HR/SQFT.)					
					41.58					
					SQFT/PERSON					
					105.00					
					TONS PER SQFT					
					0.01					
					CFM PER SQFT					
					1.90					
					TONS/PERSON					
					0.66					
					DEHUMIDIFIED CFM/TON					
					302.47					
					AREA PER TON					
					159.03					
INTERNAL SENSIBLE LOAD										
PEOPLE	2	245	490							
APPL.	500	3.4	1700							
LIGHTS	315	3.4	1.25	1339						
FOOD	0	60	0							
SUB TOTAL					7937					
LEAK LOSS +SAFETY FACTOR=5%					397					
ROOM SENSIBLE HEAT					8731					

SUBJECT : HEAT LOAD SUMMARY SHEET										
PROJECT :		INCOME TAX OFFICE GROUND FLOOR								
SR.	DISCRPTION	Area	Occupancy	WATTS	Fresh air	APPL.	Dehumidified	Tonnage	Cfm/HP	Tonnage
		Sq.ft.	Nos.	Sq.ft.	CFM	WATTS.	air	REQ. (TR)		HP
1	STAFF AREA - 1	1400	30	1.5	513	5000	3314	10.3	13.3	12.5
2	DCIT - 1	200	7	1.5	73	250	398	1.4	1.6	1.7
3	DCIT - 2	200	7	1.5	73	250	398	1.4	1.6	1.7
4	ITO - 1	190	6	2	70	250	545	1.6	2.2	1.9
5	ITO - 2	190	6	2	70	250	413	1.4	1.7	1.7
6	ITO - 3	190	6	2	70	250	507	1.5	2.0	1.9
7	ITO - 4	190	6	2	70	250	530	1.6	2.1	1.9
8	STAFF AREA - 2	1200	30	2	440	5000	3180	9.6	12.7	11.5
9	CIT A	270	10	2	100	250	745	2.3	3.0	2.7
10	AO AND PSA	240	6	2	88	500	602	1.9	2.4	2.2
11	JCTI-1	290	10	2	106	250	832	2.5	3.3	3.0
12	ADDL JCTI- 1	270	10	2	100	250	660	2.1	2.6	2.5
13	CIT (B)	270	10	2	100	250	746	2.3	3.0	2.7
14	AO AND PS (B)	210	2	2	77	500	399	1.3	1.6	1.6
	TOTAL	5310	146	21	1950	13500	13271	41	53	50



CHAPTER 08

8. PHOTOGRAPHY:



Figure 8-1. Project visit with staff



Figure 8-2. Outdoor Unit



Figure 8-3 ODU



Figure 8-4 Raffinates



Figure 8-5. Component of ODU



Figure 8-6. Cassette



Figure 8-7.IDU Cassette



Figure 8-8.Scroll Compressor



Figure 8-9.False Ceiling for IDU Installation



Figure 8-10. Inventory



Figure 8-11. Grill of IDU

CHAPTER 09

9. FUTURE SCOPE & CONCLUSION

9.1. Future Scope:

A new refrigerant detection and management system works with VRF (Variable Refrigerant Flow) air conditioning systems. In the unlikely event of a refrigerant leak, it shuts down the specific section of pipework involved, while enabling the rest of the system to continue operating as normal.

The VRF systems that are out today will undoubtedly be improved as the popularity of this system continues to increase and competition exists between manufacturers to produce the best product. In the meantime, it is best to study the operating principles of what's already out there so that the performance of these installed systems can be optimized through proper design, installation and commissioning.

The overall efficiency, design flexibility, and total life cycle cost of variable refrigerant flow (VRF) systems are driving growth of the technology in the HVAC market. Such growth is evidenced by a recent report from Markets and Markets, which reports the global VRF market is projected to reach approximately \$9.65 billion by 2021, registering a compound annual growth rate (CAGR) of 10.8 percent between 2016 and 2021.

We should get better efficient system by calculating heat & cooling load on TOSHIBA SMMS7 software. This software is fully automated due to which we can calculating heat load of complicate space easily. We will also be using Carrier HAP software for the calculating the heat & cooling load which is fully automated.

9.2. Conclusion:

The VRF system has been designed successfully considering the required indoor condition. proper pipe dimensions and material has been selected. indoor and outdoor units as per requirement are selected.



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